

Sensor and Simulation Notes

Note 62

A Parameter Study of Open-Circuited and
Short-Circuited Transmission Line Simulation for
Buried Structures of EMP Sensor and Simulation Note XXII

by

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ABSTRACT

The magnitude of open-circuited and short-circuited transmission line impedances versus frequency are graphed for various values of the geometric factor, depth of the transmission line and ground conductivity. A computer code that produces the plots for any value of the parameters is described and listed.

I. INTRODUCTION

In this note the influence of three parameters on the frequency versus the magnitude of the impedance for a buried transmission line simulator is studied; the study is based on an analysis by Carl E. Baum.* The simulator consists of two parallel plates of width $2a$, separated by a distance of $2b$, and a depth into the ground of ℓ . The geometry of the configuration is shown in Figure 1.

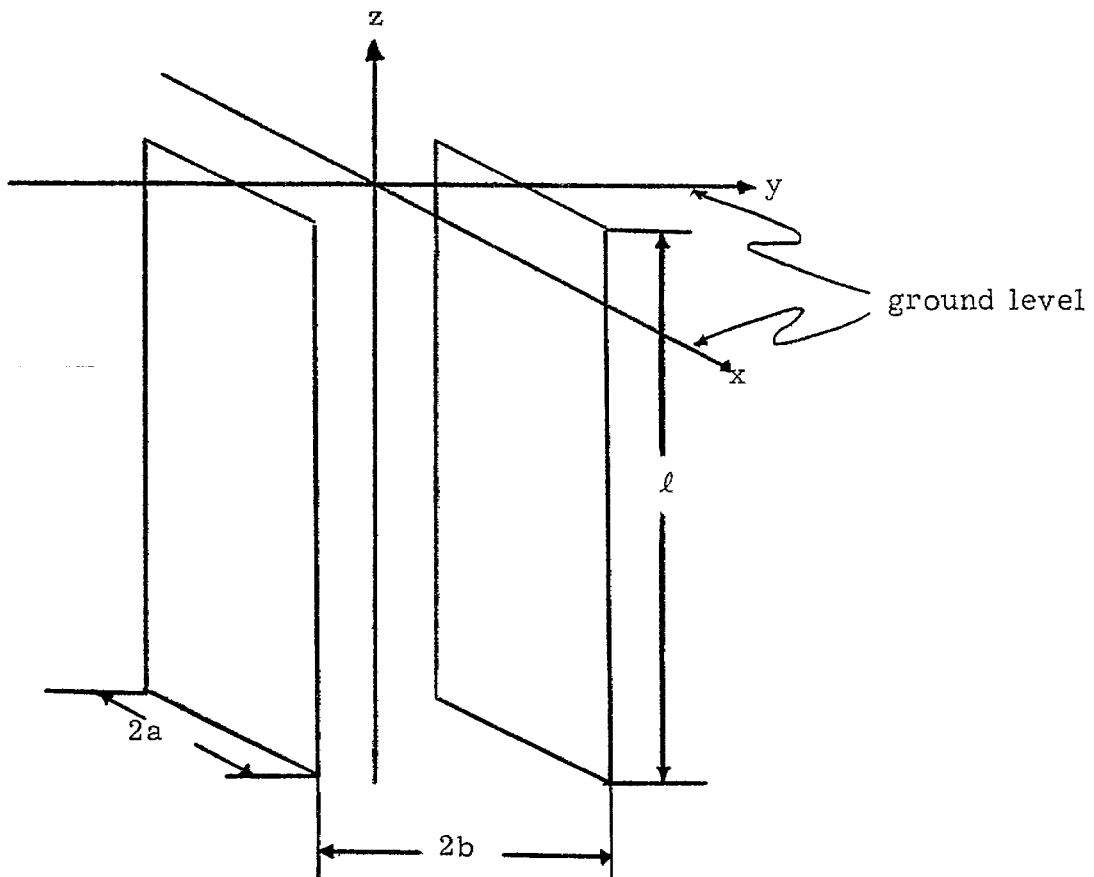


Figure 1

* C. E. Baum, "A Transmission Line EMP Simulation Technique for Buried Structures," EMP Sensor and Simulation Note XXII, June 6, 1966.

The limit of our concern in this note is to compare frequency to the impedance of the open-circuited and short-circuited transmission line for various plate-depths, ground conductivity and geometric factors. A computer code that can easily be used to produce graphs for any value of the parameters is included since not all interesting combinations can be presented here.

II. OPERATION

General

The plots contained in this note were produced on the Calcomp Plotter. Each graph is logarithmic vertically and logarithmic horizontally with 150 points plotted along each curve. The heading of each graph contains the three parameters, that is, plate depth (L), conductivity, and the geometric factor.

Practically, it is more desirable to describe the geometry of the simulator in terms of the ratio of the plate separation to the plate width (b/a) than in terms of the geometric factor (f_g). For this reason, provisions have been made to list b/a to clarify the geometry. However, it should be noted that f_g and not b/a is necessary for the calculations in the program. The code does not calculate f_g from b/a . If the geometric factor is not known for a given b/a it can be determined with the computer code described in EMP Sensor and Simulation Note LII¹.

The impedances for the two curves of each graph are given by equations (1) and (2), below. These values are computed and plotted for various combinations of the parameters. Since these quantities are generally complex, the magnitude of each is plotted against frequency. The frequency is in cycles per second. The curves are distinguished by tagging

* T. L. Brown and K. D. Granzow, "A Parameter Study of Two-Plate Transmission Line Simulators of EMP Sensor and Simulation Note XXI," EMP Sensor and Simulation Note LII, April 19, 1968.

them with $|Z_{L_o}|$ and $|Z_{L_s}|$ for the magnitude of the open-circuited and magnitude of the short-circuited transmission line impedance, respectively.

Accepting from Note XXII, along with their restrictions, we have the open-circuited transmission line impedance

$$Z_{L_o} = Z_{L_\infty} \frac{1 + e^{-j2k\ell}}{1 - e^{-j2k\ell}} \quad (1)$$

and the short-circuited transmission line impedance

$$Z_{L_s} = Z_{L_\infty} \frac{1 - e^{-j2k\ell}}{1 + e^{-j2k\ell}} \quad (2)$$

The impedance of an infinite or ideal transmission line is given by

$$Z_{L_\infty} = f_g \frac{1 + j}{\delta\sigma} \quad (3)$$

where the propagation constant, k , is

$$k \approx \frac{1 - j}{\delta} \quad (4)$$

and skin depth is

$$\delta \approx \sqrt{\frac{2}{\omega\mu\sigma}} = \sqrt{\frac{1}{\pi f\mu\sigma}} \quad (5)$$

A description of the variables is as follows:

<u>Variable</u>	<u>Designation</u>	<u>Unit of Measure</u>
μ	Ground permeability	$\mu = \mu_0 = 4\pi \times 10^{-7}$ henrys/meter
f_g	Geometric factor	
σ	Ground conductivity	mhos/meter
k	Propagation constant	
f	Frequency	cycles/second
l	Plate depth	meters
δ	Skin depth	

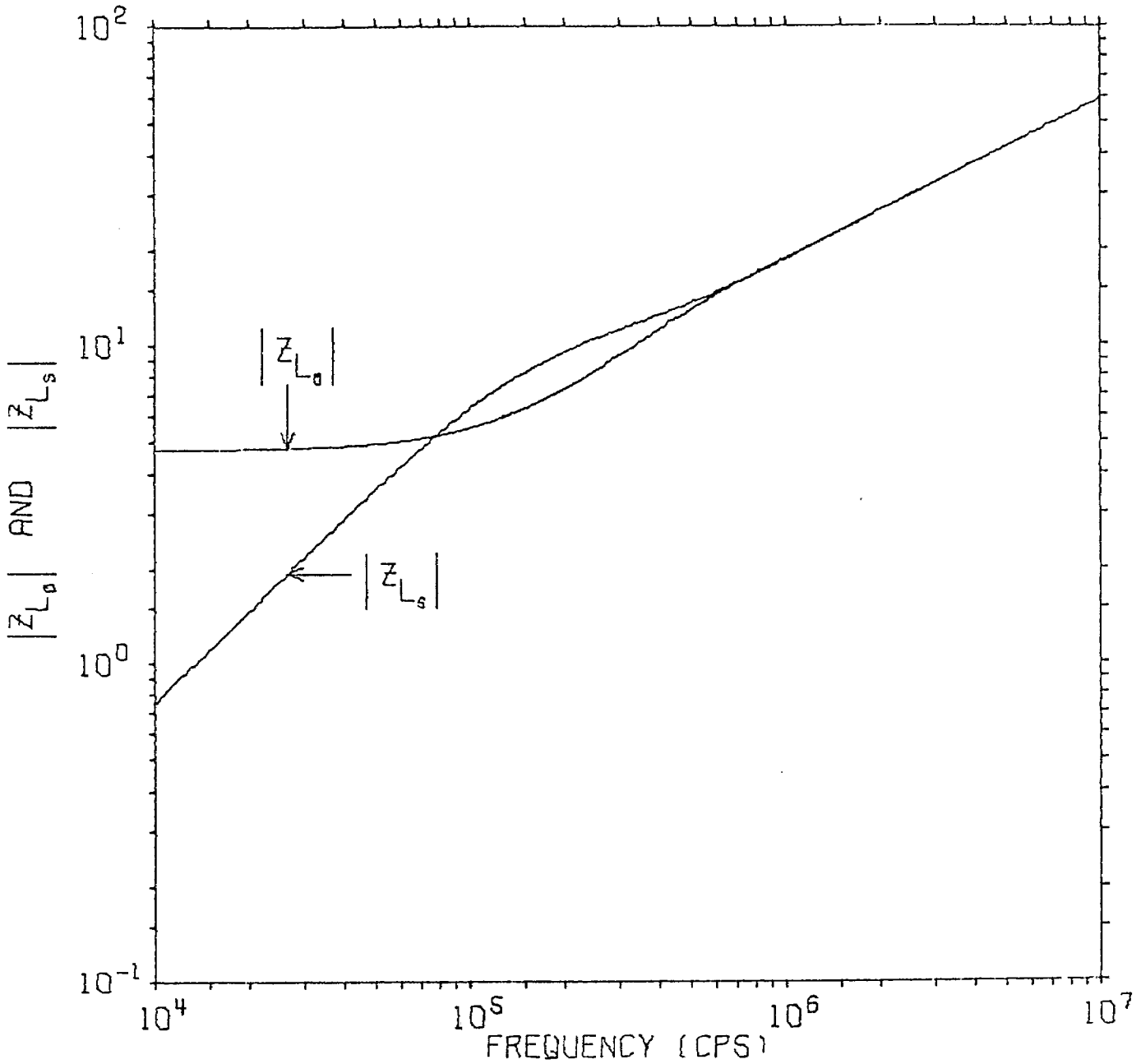
The table below summarizes the graphs found in this note.

<u>f_g</u>	<u>b/a</u>	<u>l</u>	<u>σ</u>
.47263959	1.0	20.0	5.00×10^{-3}
		20.0	8.00×10^{-3}
		20.0	1.10×10^{-2}
		20.0	3.00×10^{-2}
		40.0	5.00×10^{-3}
		40.0	8.00×10^{-3}
		40.0	1.10×10^{-2}
		40.0	3.00×10^{-2}
		60.0	5.00×10^{-3}
		60.0	8.00×10^{-3}
		60.0	1.10×10^{-2}
		60.0	3.00×10^{-2}
		80.0	5.00×10^{-3}
		80.0	8.00×10^{-3}
		80.0	1.10×10^{-2}
		80.0	3.00×10^{-2}

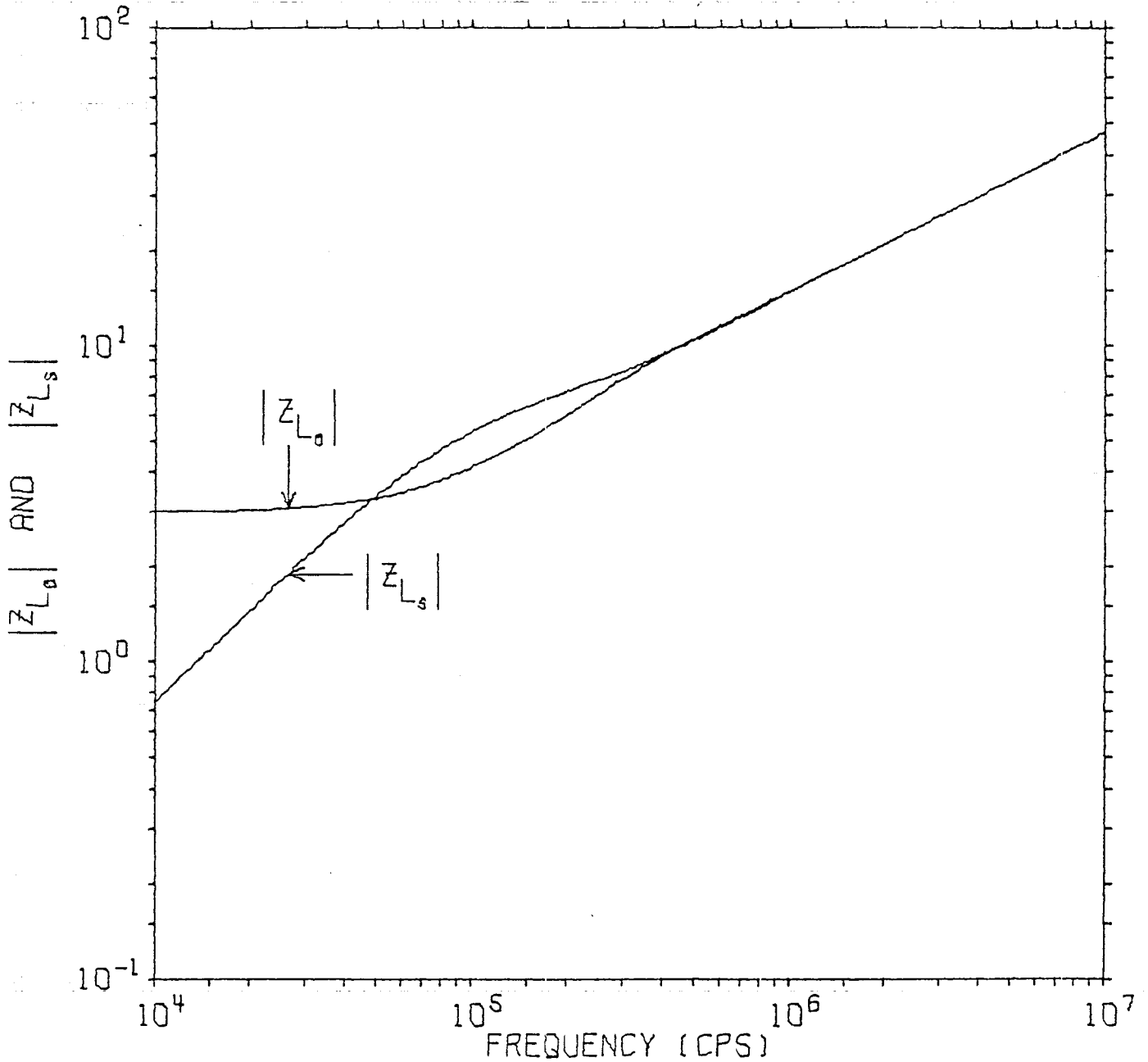
$\frac{f}{g}$	$\frac{b}{a}$	$\underline{\ell}$	$\underline{\sigma}$
.47263959	1.0	100.0	5.00×10^{-3}
		100.0	8.00×10^{-3}
		100.0	1.10×10^{-2}
		100.0	3.00×10^{-2}

The following graphs were reproduced directly from the Calcomp plots.

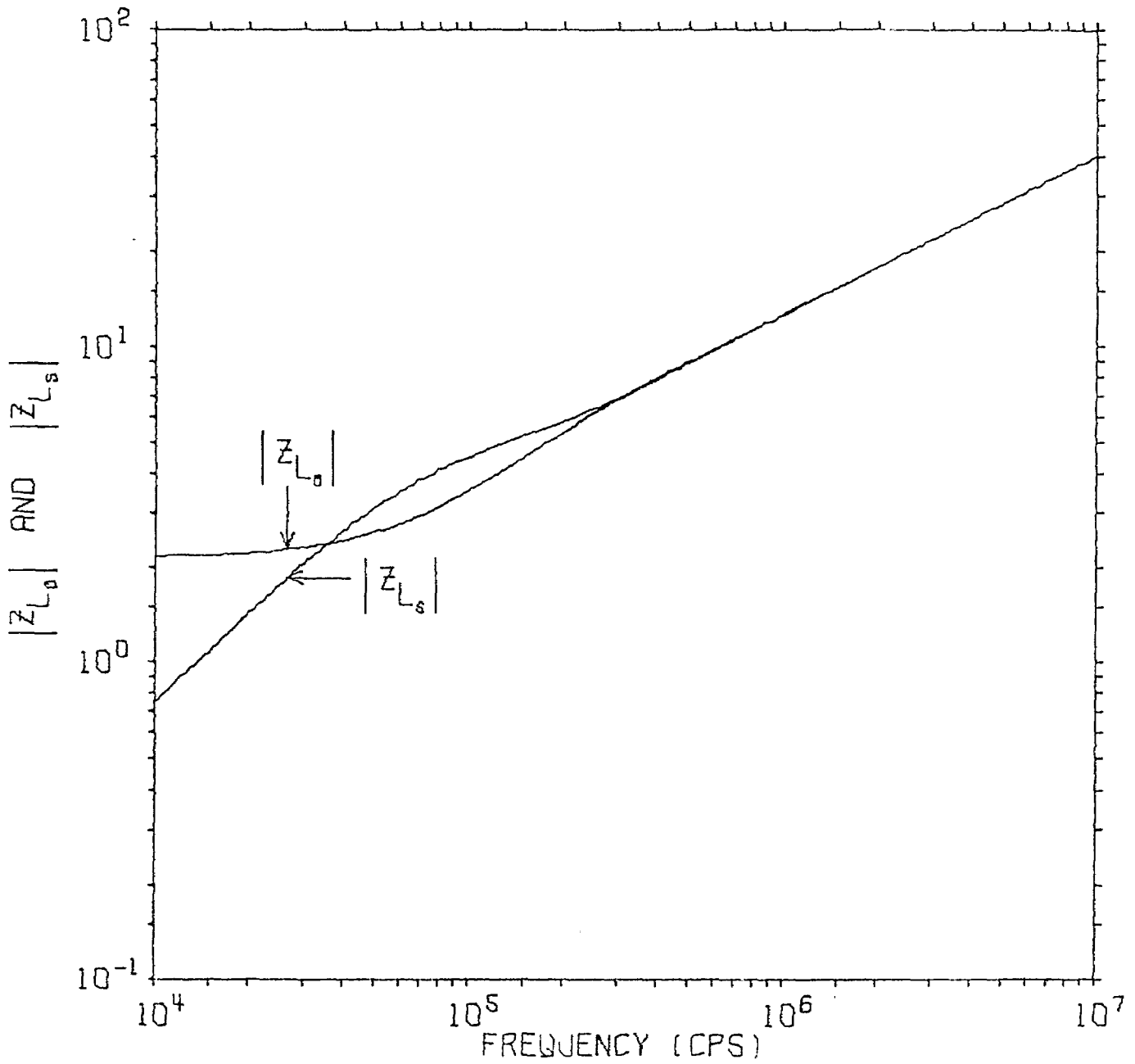
MAGNITUDE OF OPEN-CIRCUITED AND SHORT-CIRCUITED TRANSMISSION
 LINE IMPEDANCE VERSUS FREQUENCY FOR
 $L = 20.0$ METERS, CONDUCTIVITY = $5.00E-03$ MHOS/METER
 $FG = .473$ ($B/A = 1.00$)



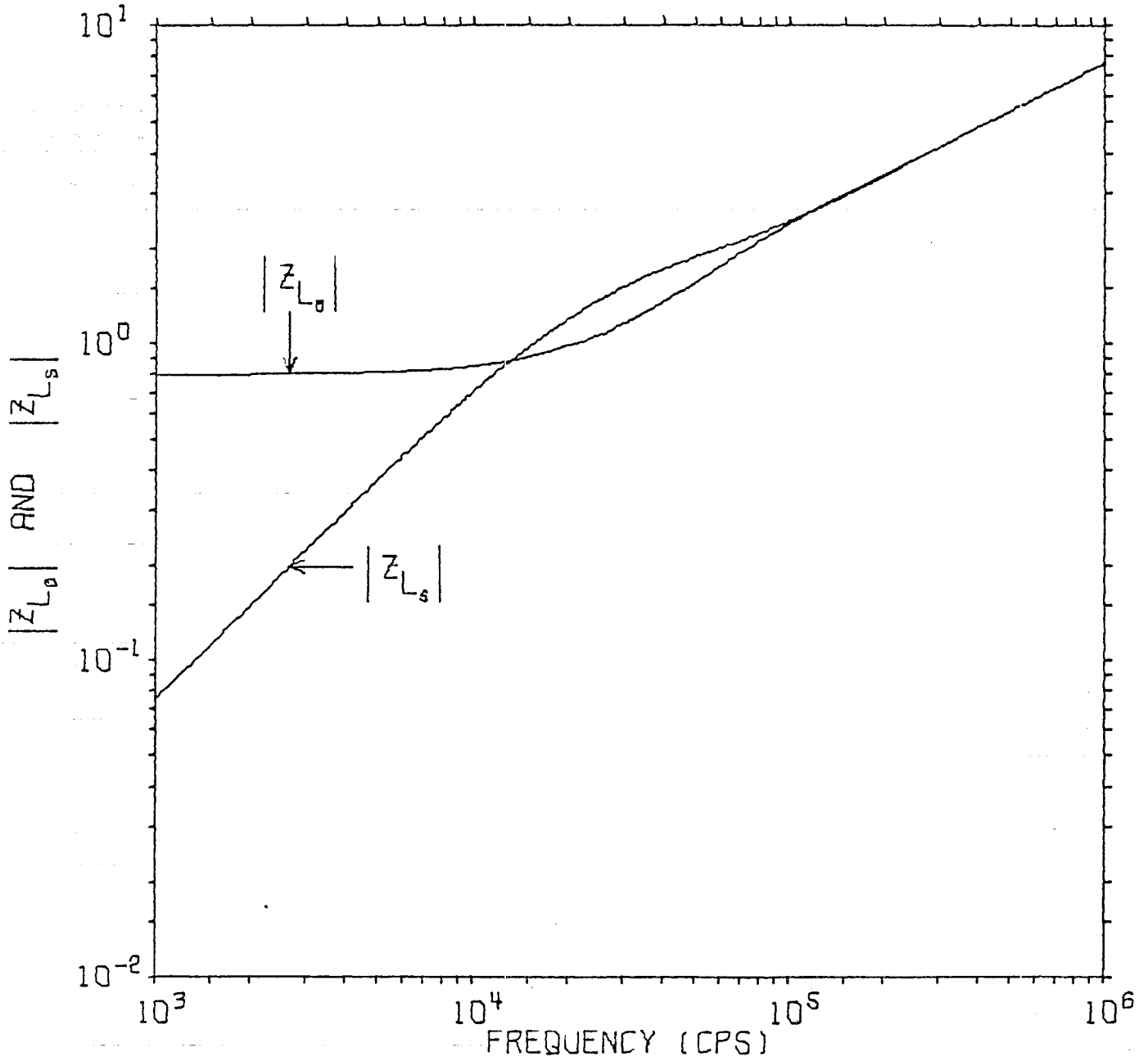
MAGNITUDE OF OPEN-CIRCUITED AND SHORT-CIRCUITED TRANSMISSION
 LINE IMPEDANCE VERSUS FREQUENCY FOR
 $L = 20.0$ METERS, CONDUCTIVITY = $8.00E-03$ MHOS/METER
 $FG = .473$ ($B/A = 1.00$)



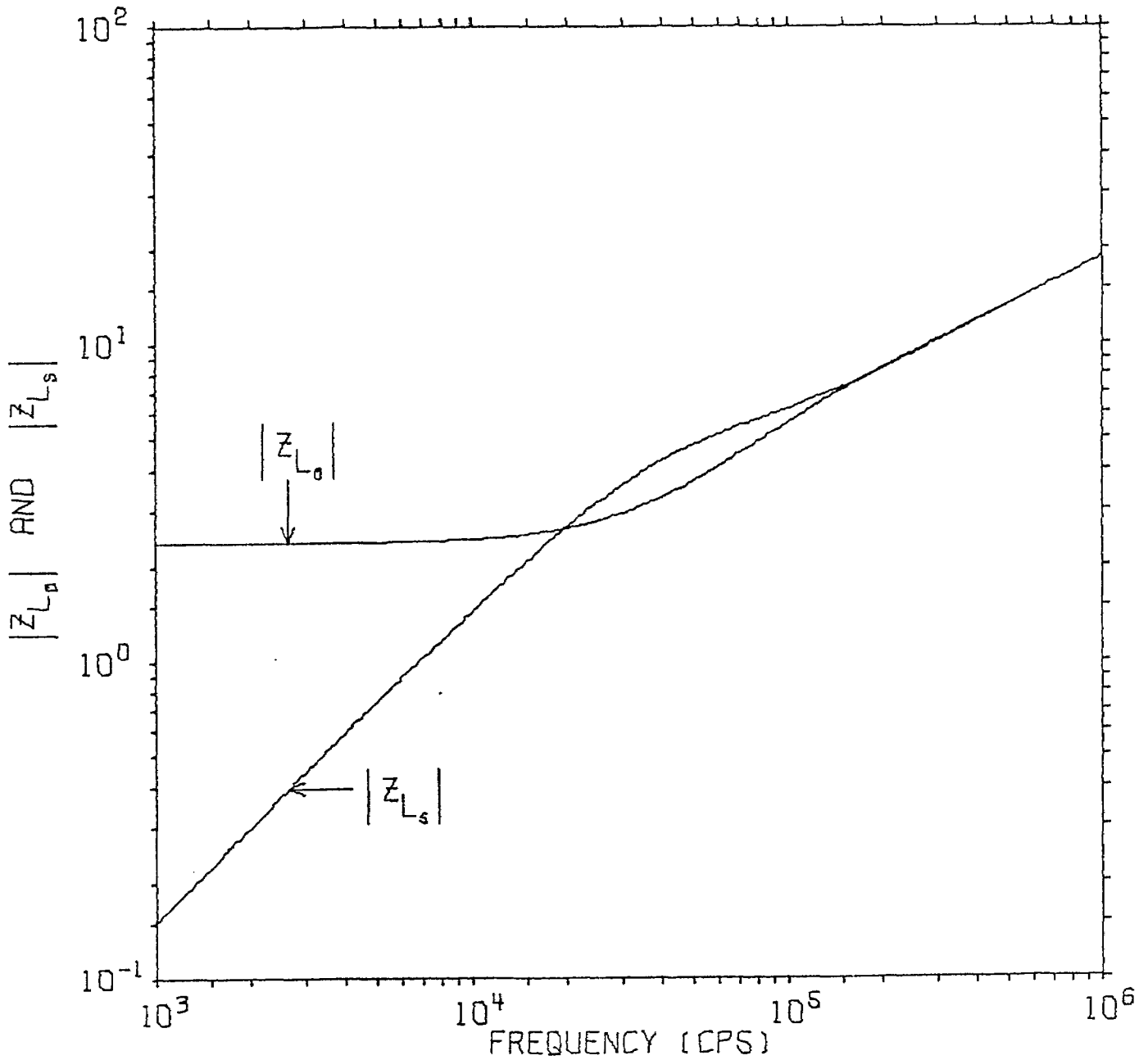
MAGNITUDE OF OPEN-CIRCUITED AND SHORT-CIRCUITED TRANSMISSION
LINE IMPEDANCE VERSUS FREQUENCY FOR
L = 20.0 METERS. CONDUCTIVITY = 1.10E-02 MHOS/METER
FG = .473 (B/A = 1.00)



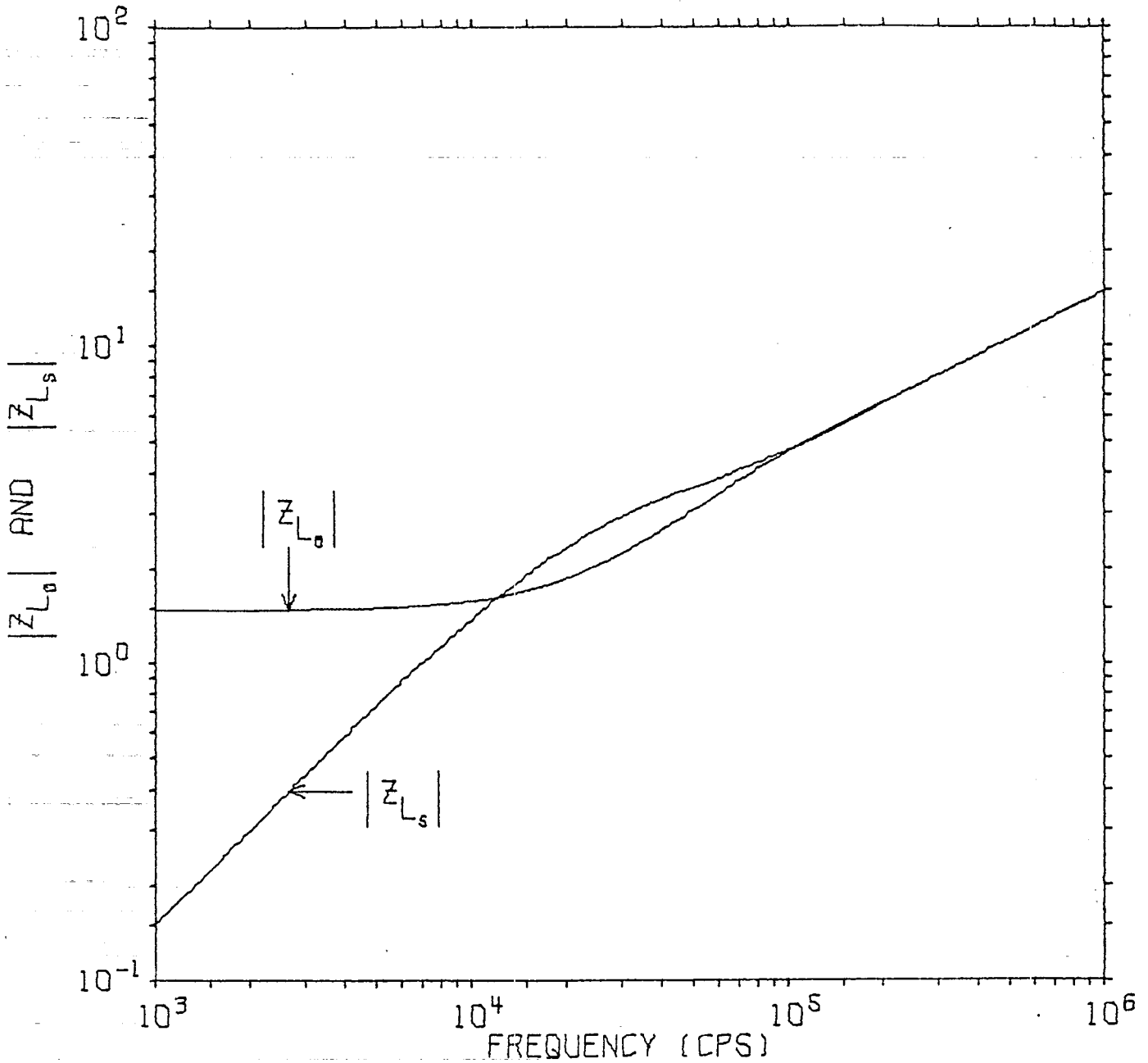
MAGNITUDE OF OPEN-CIRCUITED AND SHORT CIRCUITED TRANSMISSION
 LINE IMPEDANCE VERSUS FREQUENCY FOR
 L = 20.0 METERS, CONDUCTIVITY = 3.00E-02 MHOS/METER
 FG = .473 (B/A = 1.00)



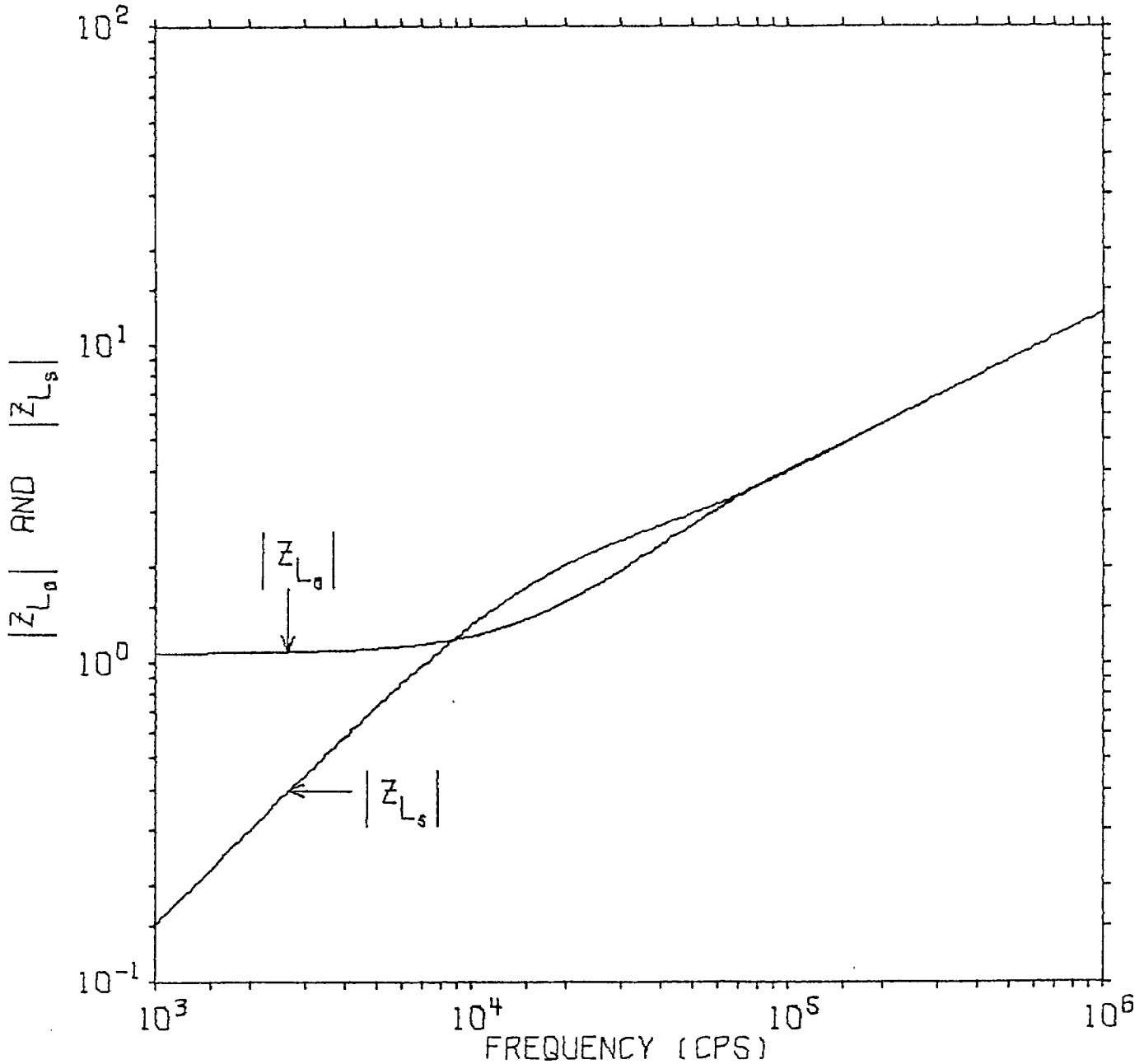
MAGNITUDE OF OPEN-CIRCUITED AND SHORT-CIRCUITED TRANSMISSION
 LINE IMPEDANCE VERSUS FREQUENCY FOR
 $L = 40.0$ METERS, CONDUCTIVITY = $5.00E-03$ MHOS/METER
 $FG = .473$ ($B/A = 1.00$)



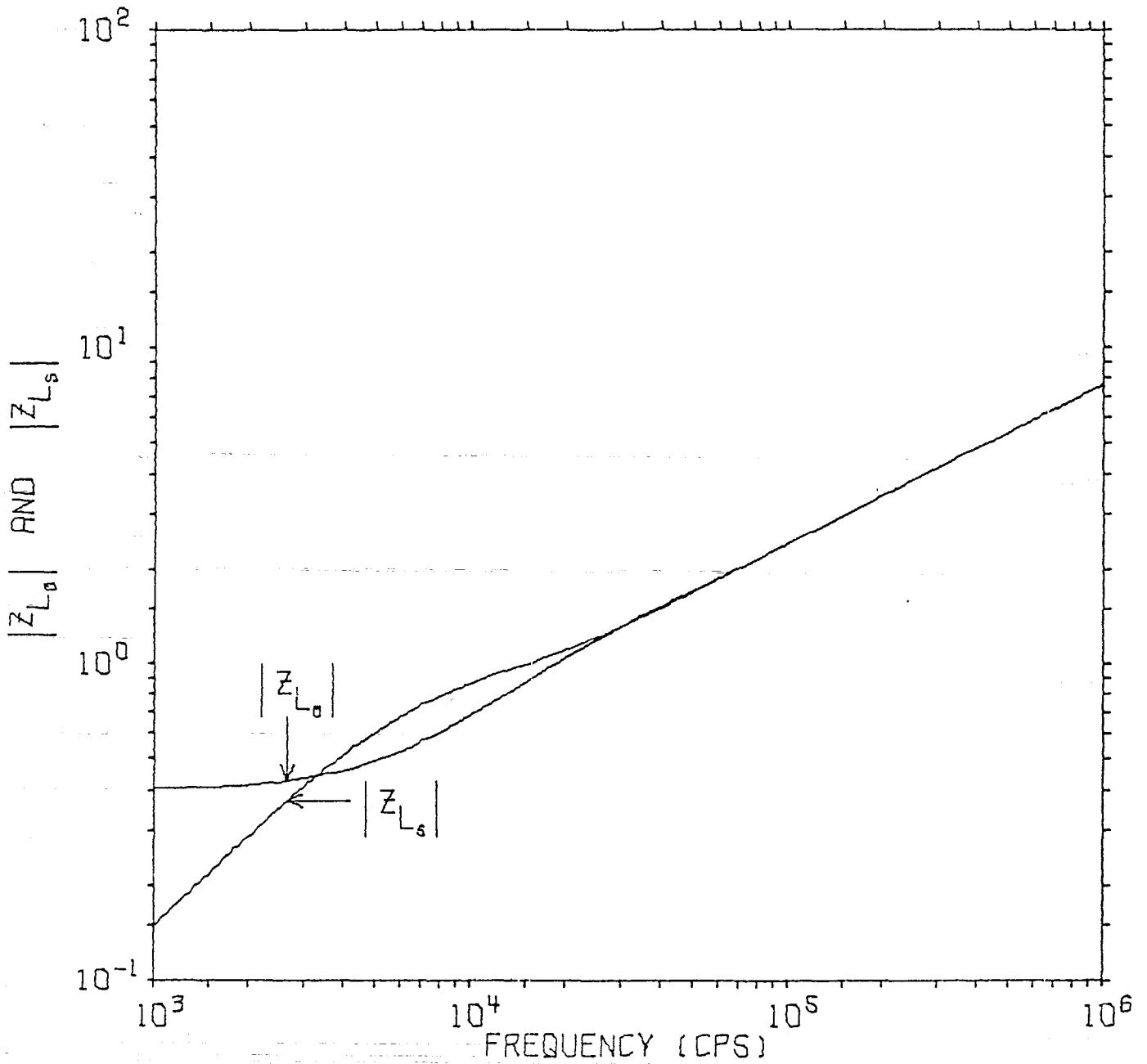
MAGNITUDE OF OPEN-CIRCUITED AND SHORT-CIRCUITED TRANSMISSION
 LINE IMPEDANCE VERSUS FREQUENCY FOR
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 $FG = .473$ ($B/A = 1.00$)



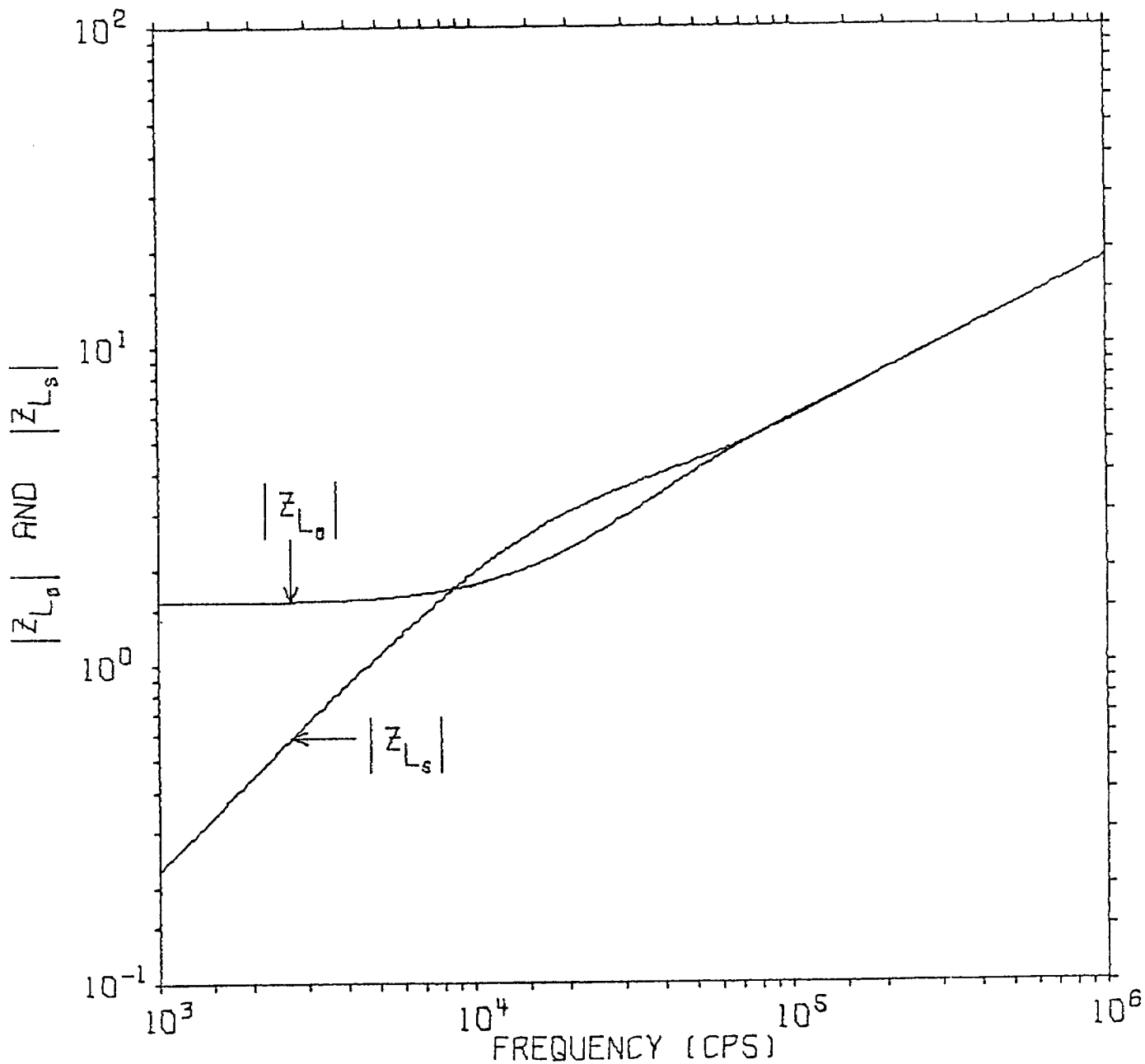
MAGNITUDE OF OPEN-CIRCUITED AND SHORT-CIRCUITED TRANSMISSION
 LINE IMPEDANCE VERSUS FREQUENCY FOR
 $L = 40.0$ METERS, CONDUCTIVITY = $1.10E-02$ MHOS/METER
 $FG = .473$ ($B/A = 1.00$)



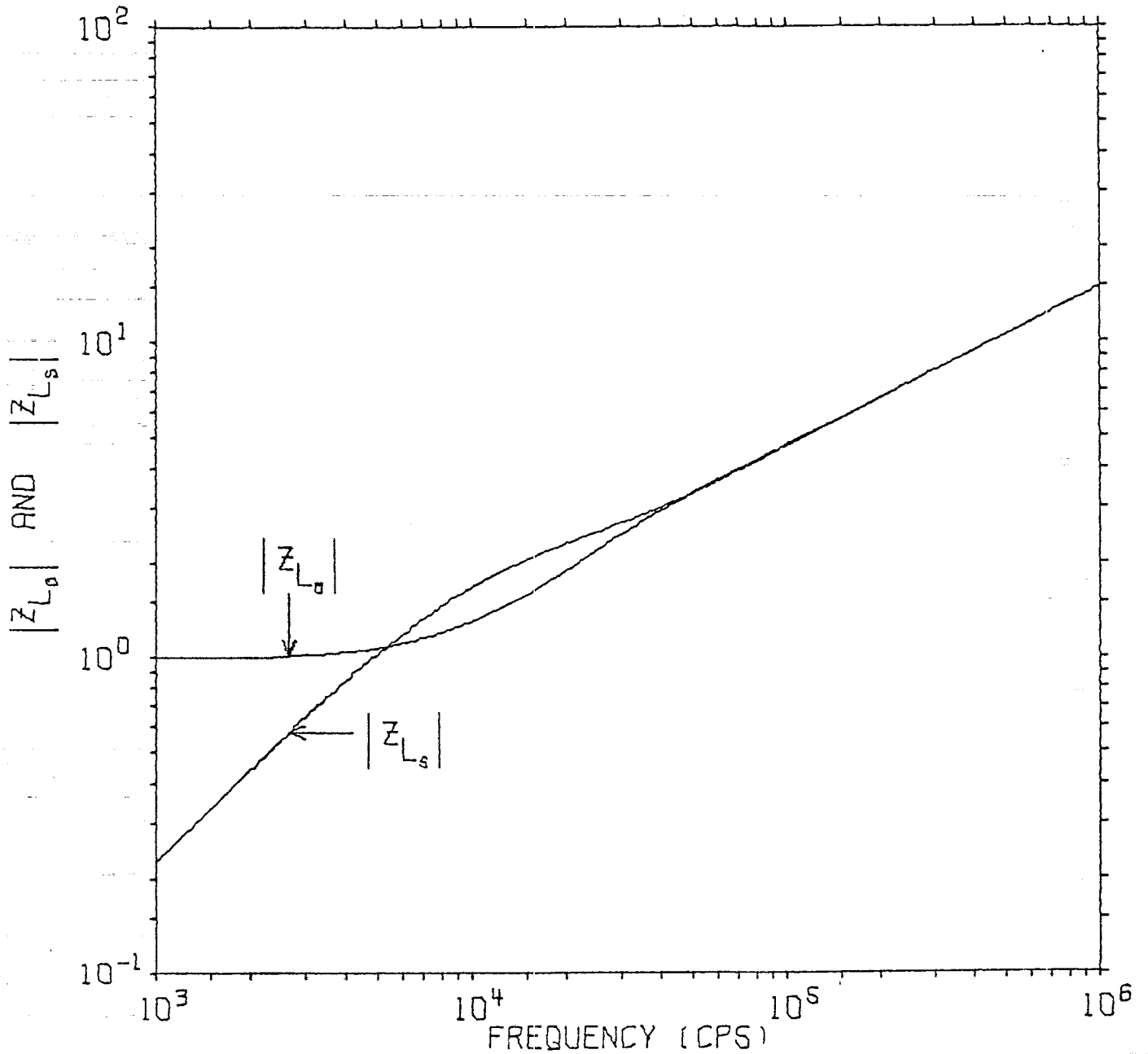
MAGNITUDE OF OPEN-CIRCUITED AND SHORT-CIRCUITED TRANSMISSION
 LINE IMPEDANCE VERSUS FREQUENCY FOR
 $L = 40.0$ METERS, CONDUCTIVITY $= 3.00E-02$ MHOS/METER
 $FG = .473$ ($B/A = 1.00$)



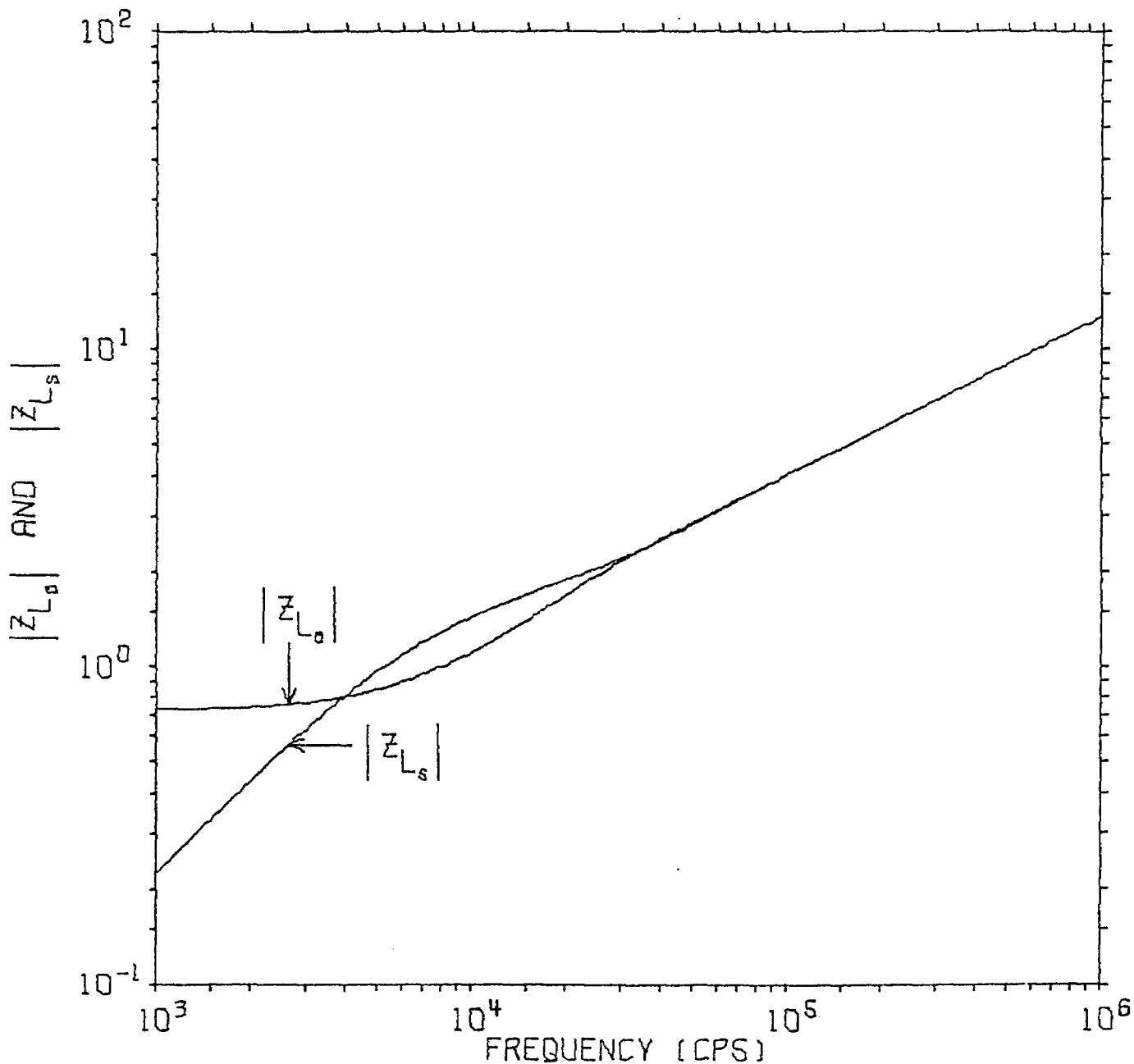
MAGNITUDE OF OPEN-CIRCUITED AND SHORT-CIRCUITED TRANSMISSION
 LINE IMPEDANCE VERSUS FREQUENCY FOR
 L = 60.0 METERS, CONDUCTIVITY = 5.00E-03 MHOS/METER
 FG = .473 (B/A = 1.00)



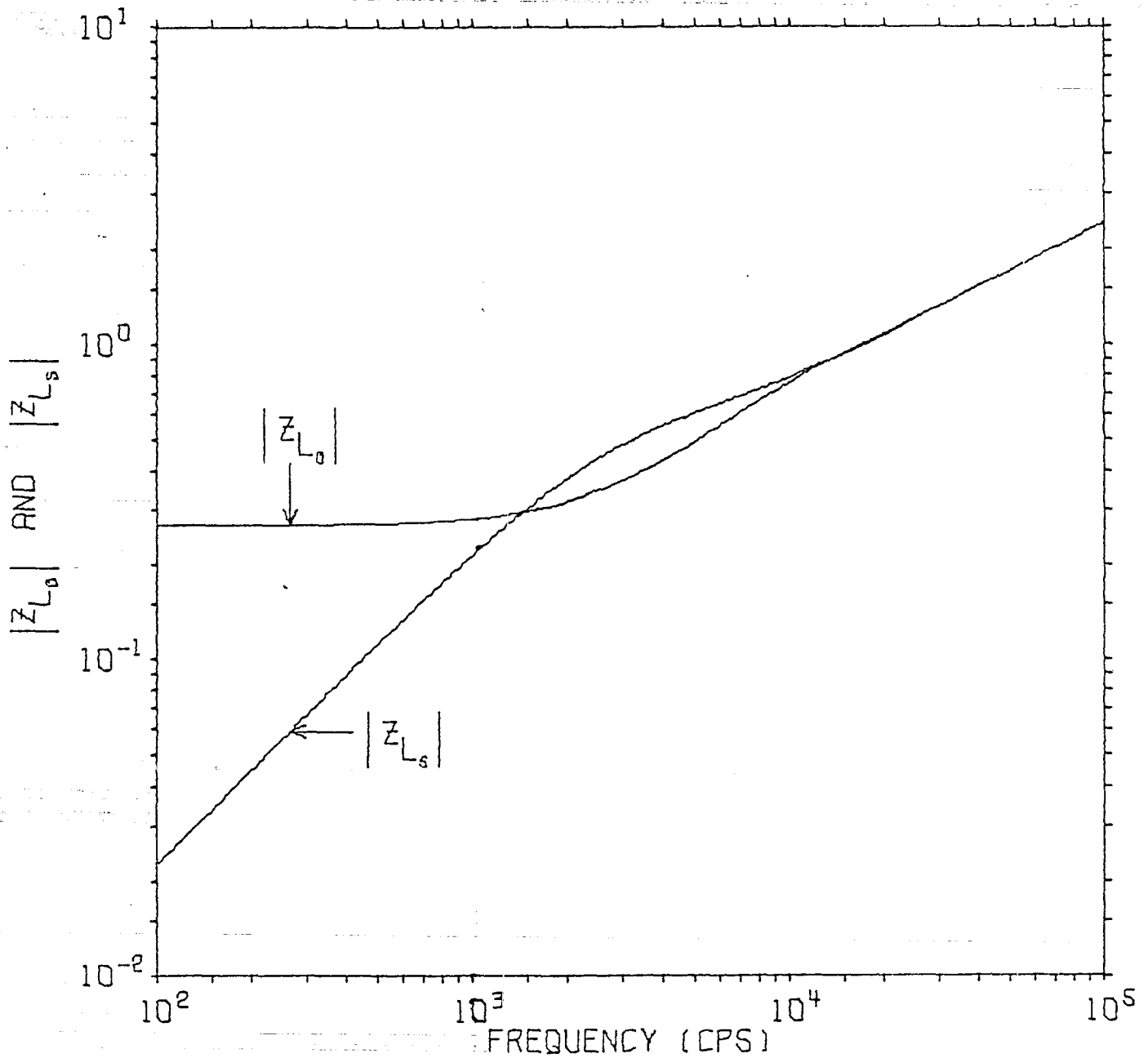
MAGNITUDE OF OPEN-CIRCUITED AND SHORT-CIRCUITED TRANSMISSION
 LINE IMPEDANCE VERSUS FREQUENCY FOR
 $L = 60.0$ METERS, CONDUCTIVITY = $8.00E-03$ MHOS/METER
 $FG = .473$ ($B/A = 1.00$)



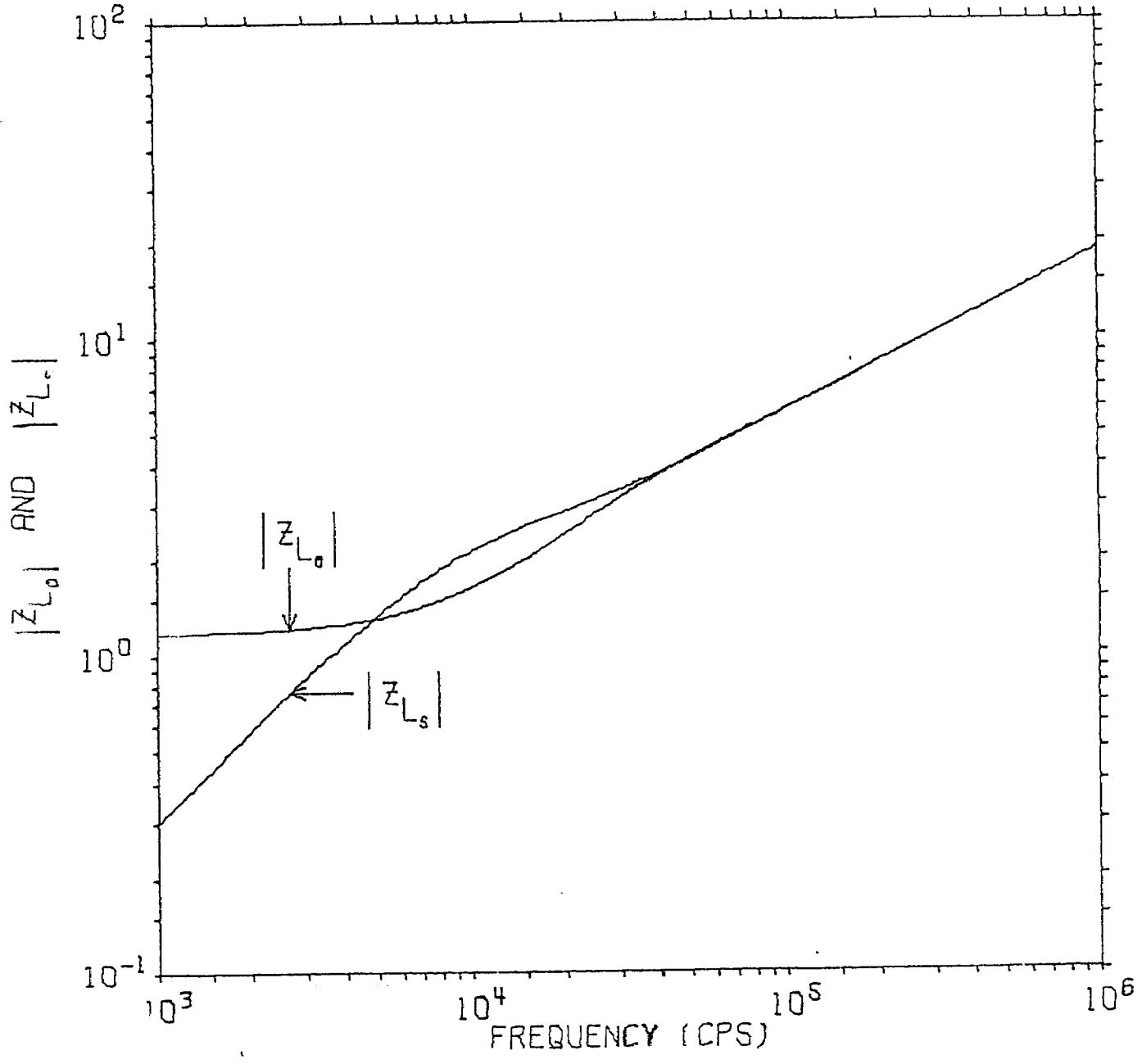
MAGNITUDE OF OPEN-CIRCUITED AND SHORT-CIRCUITED TRANSMISSION
 LINE IMPEDANCE VERSUS FREQUENCY FOR
 L = 60.0 METERS, CONDUCTIVITY = 1.10E-02 MHOS/METER
 FG = .473 (B/A = 1.00)



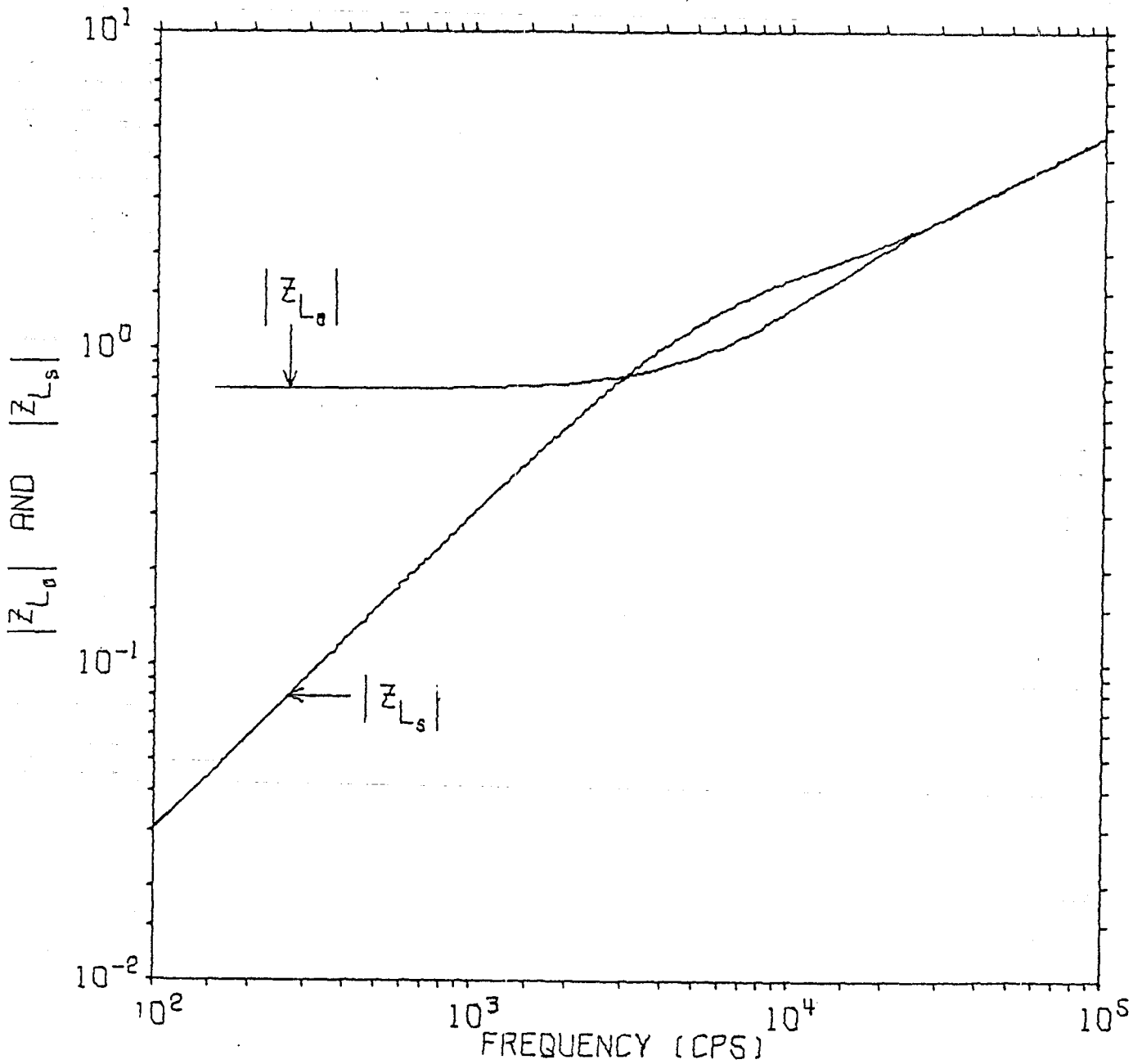
MAGNITUDE OF OPEN-CIRCUITED AND SHORT-CIRCUITED TRANSMISSION
 LINE IMPEDANCE VERSUS FREQUENCY FOR
 L = 60.0 METERS, CONDUCTIVITY = 3.00E-02 MHOS/METER
 FG = .473 (B/A = 1.00)



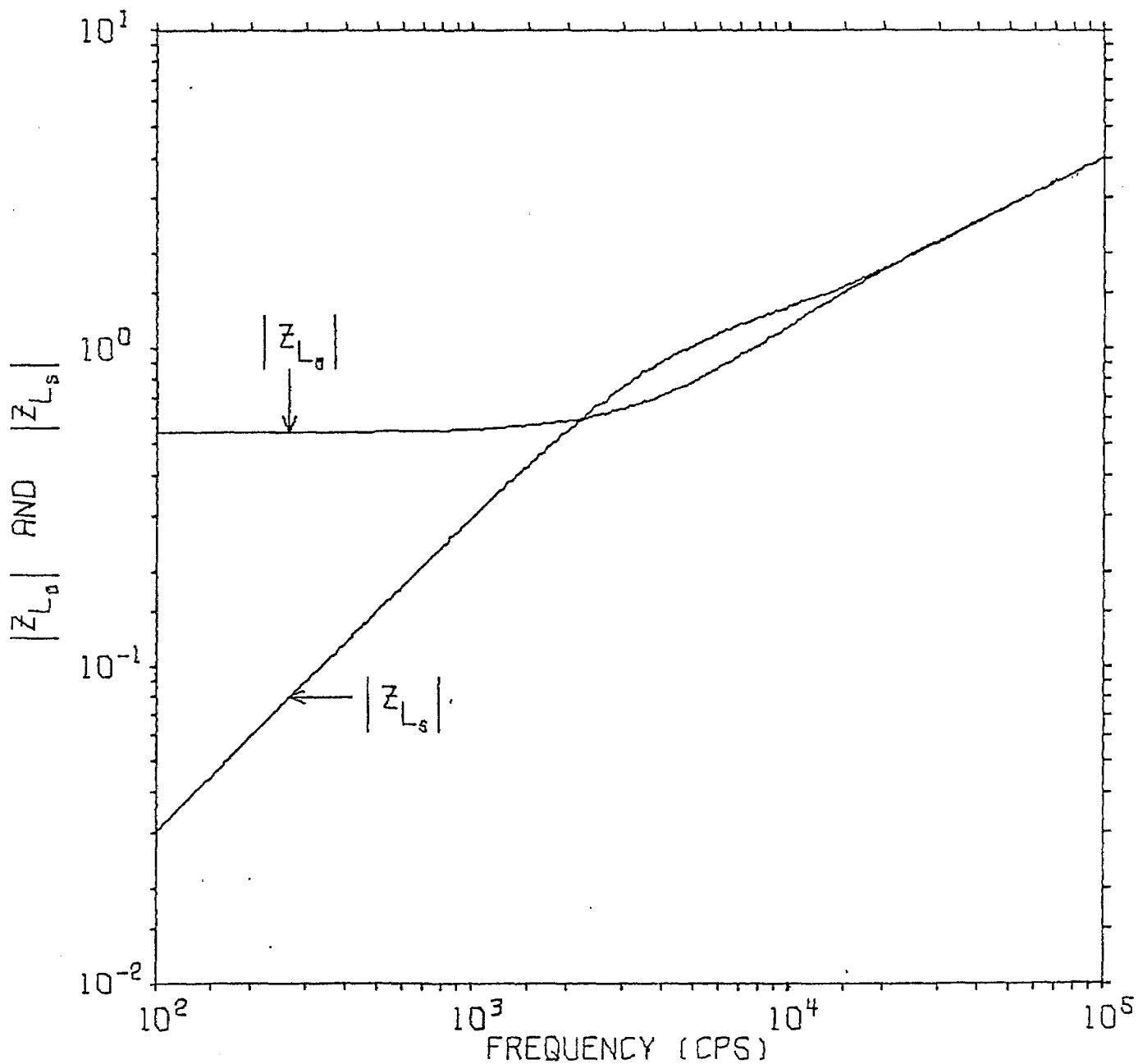
MAGNITUDE OF OPEN-CIRCUITED AND SHORT-CIRCUITED TRANSMISSION
 LINE IMPEDANCE VERSUS FREQUENCY FOR
 $L = 80.0$ METERS, CONDUCTIVITY = $5.00E-03$ MHOS/METER
 $FG = .473$ ($B/A = 1.00$)



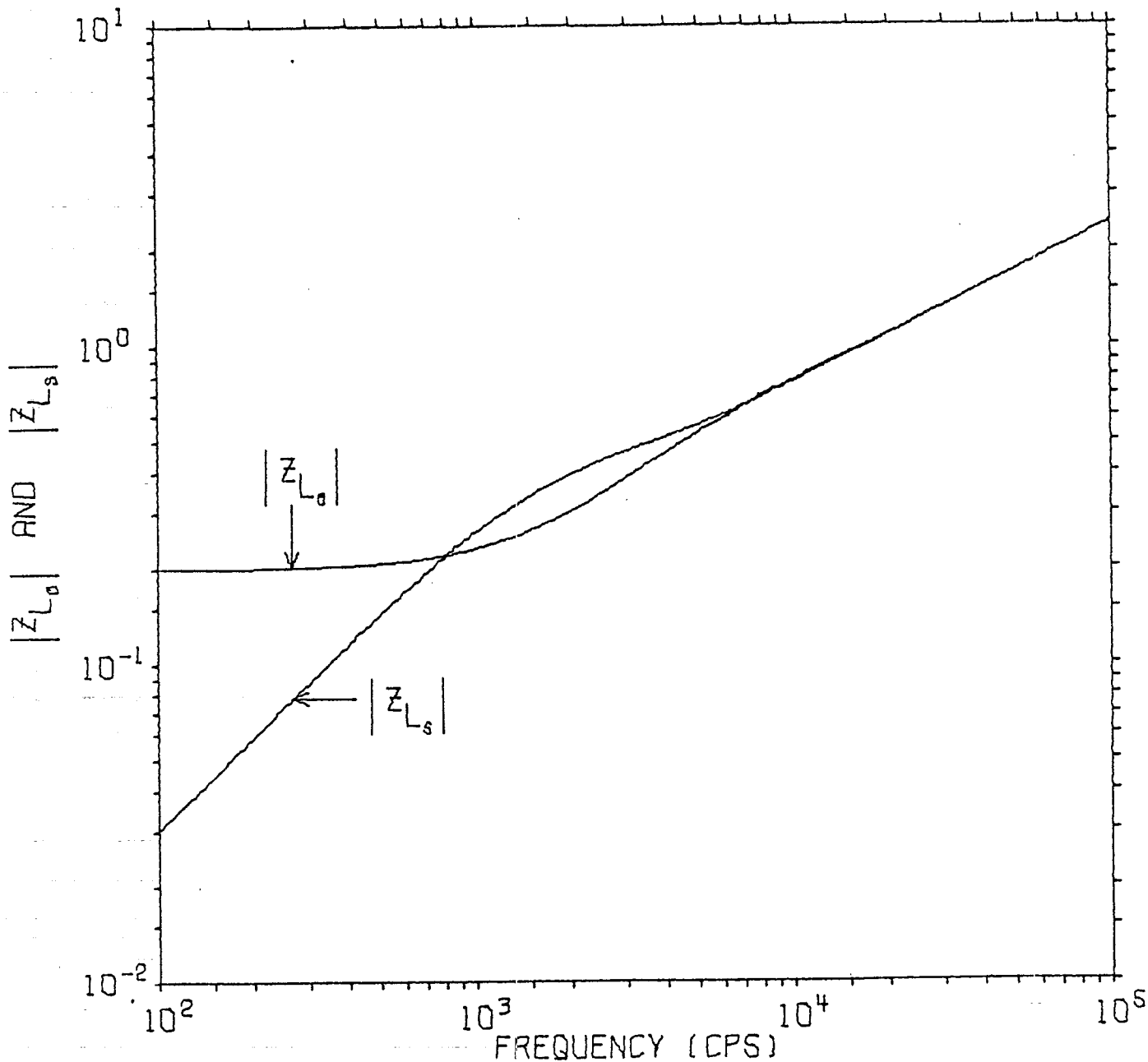
MAGNITUDE OF OPEN CIRCUITED AND SHORT-CIRCUITED TRANSMISSION
 LINE IMPEDANCE VERSUS FREQUENCY FOR
 $L = 80.0$ METERS, CONDUCTIVITY $= 8.00E-03$ MHOS/METER
 $FG = .473$ ($B/A = 1.00$)



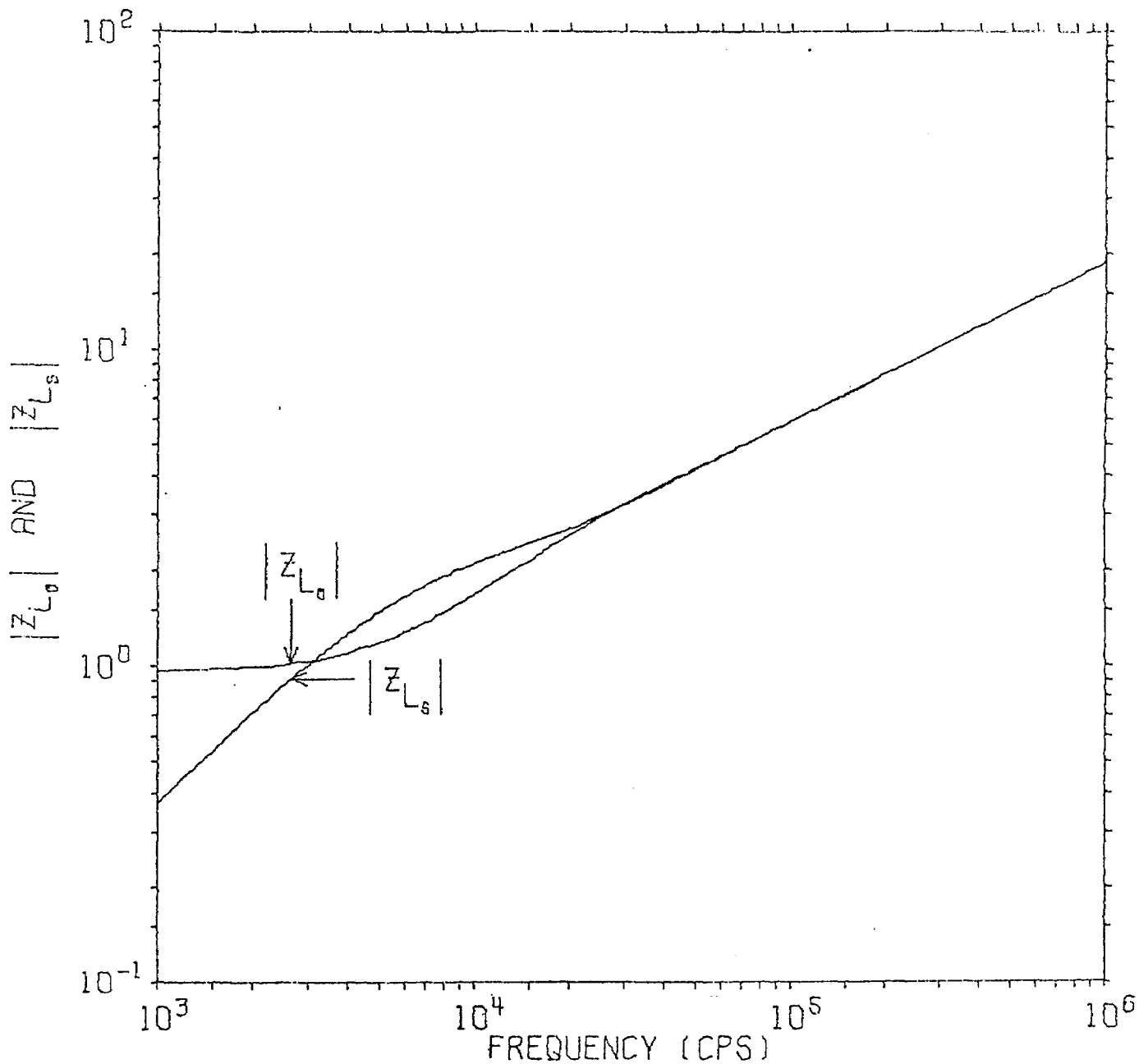
MAGNITUDE OF OPEN-CIRCUITED AND SHORT-CIRCUITED TRANSMISSION
 LINE IMPEDANCE VERSUS FREQUENCY FOR
 $L = 80.0$ METERS, CONDUCTIVITY = $1.10E-02$ MHOS/METER
 $FG = .473$ ($B/A = 1.00$)



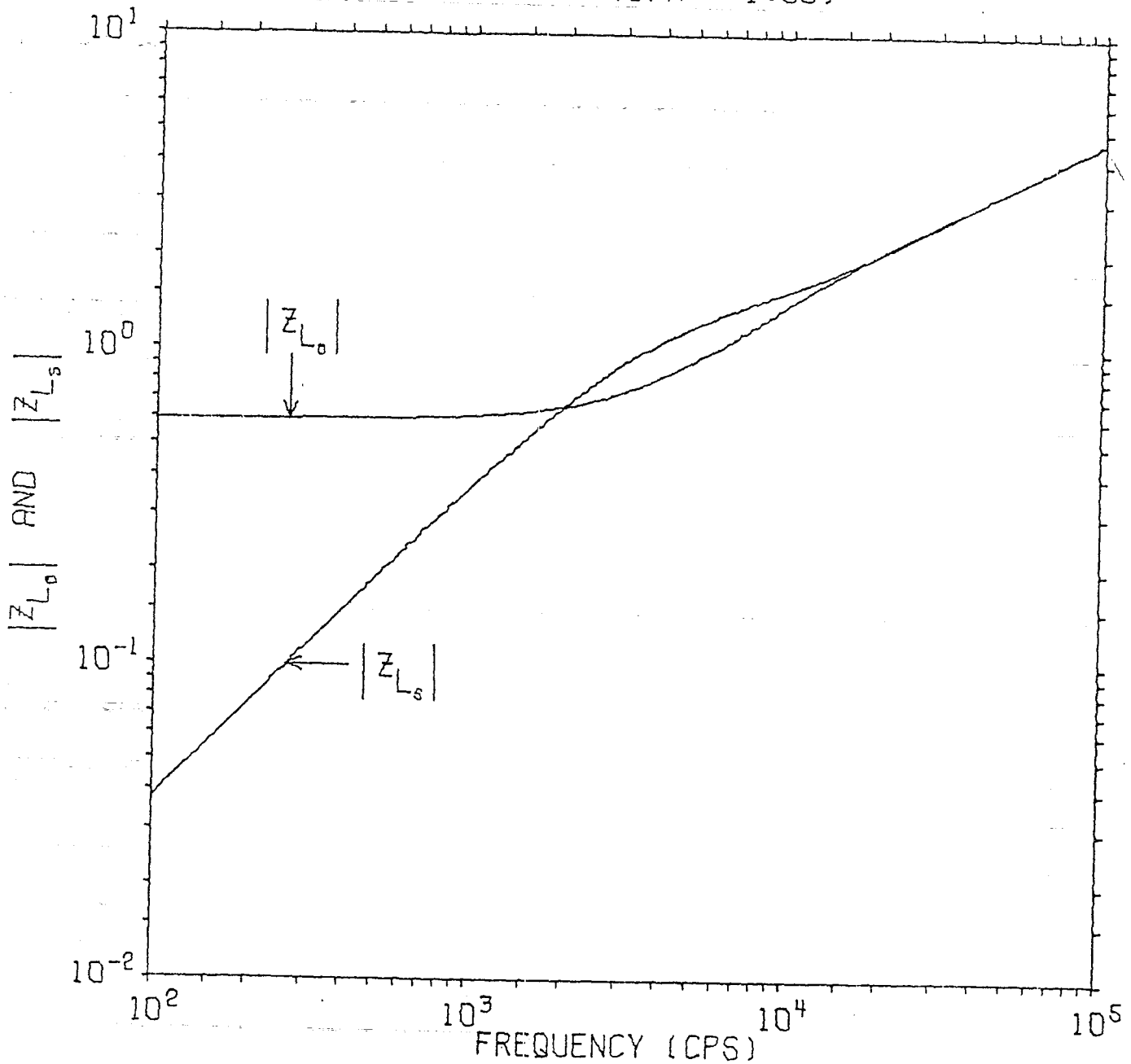
MAGNITUDE OF OPEN-CIRCUITED AND SHORT-CIRCUITED TRANSMISSION
 LINE IMPEDANCE VERSUS FREQUENCY FOR
 $L = 80.0$ METERS, CONDUCTIVITY = $3.00E-02$ MHOS/METER
 $FG = .473$ ($B/A = 1.00$)



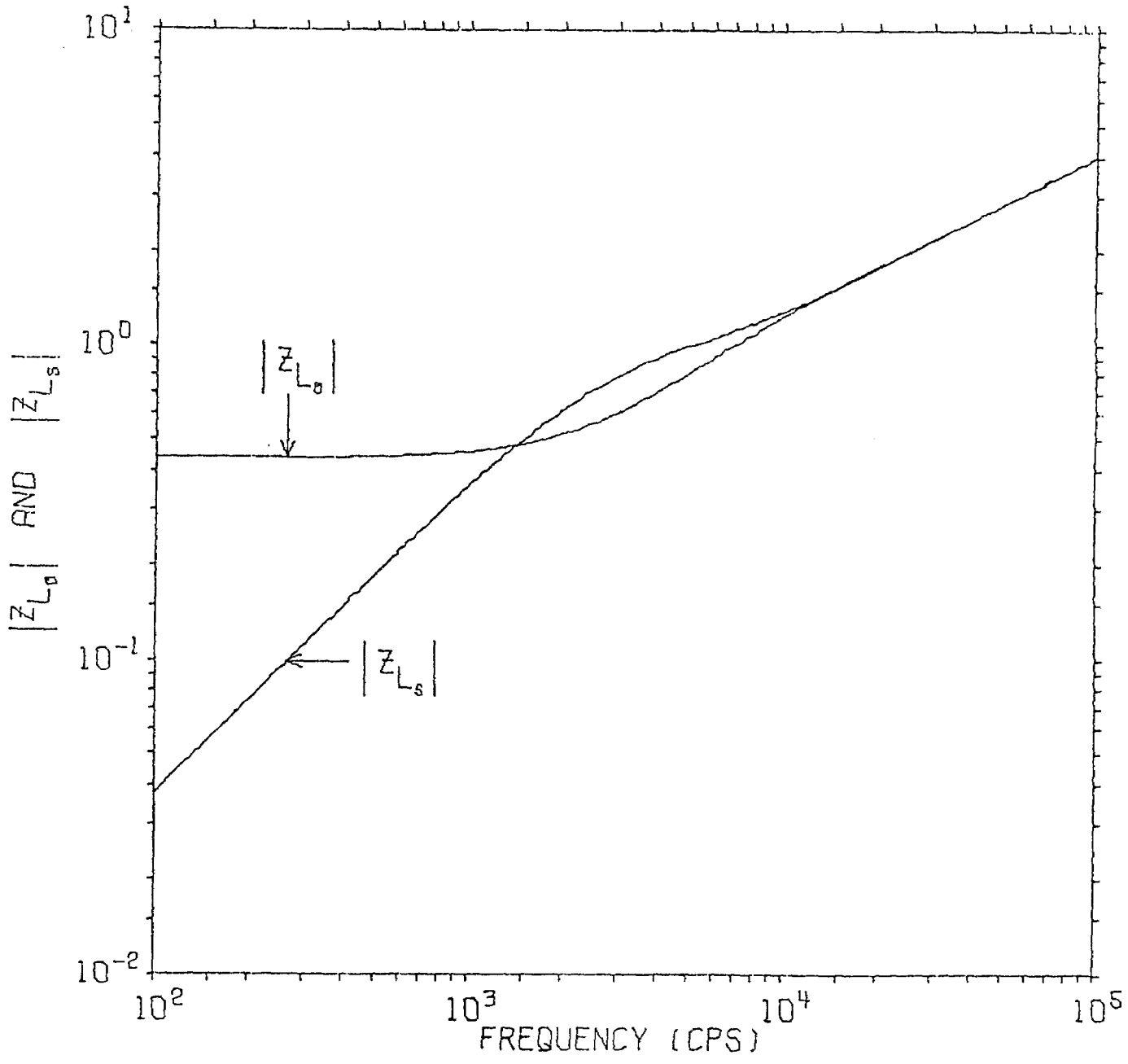
MAGNITUDE OF OPEN-CIRCUITED AND SHORT-CIRCUITED TRANSMISSION
LINE IMPEDANCE VERSUS FREQUENCY FOR
L = 100.0 METERS, CONDUCTIVITY = 5.00E-03 MHOS/METER
FG = .473 (B/A = 1.00)



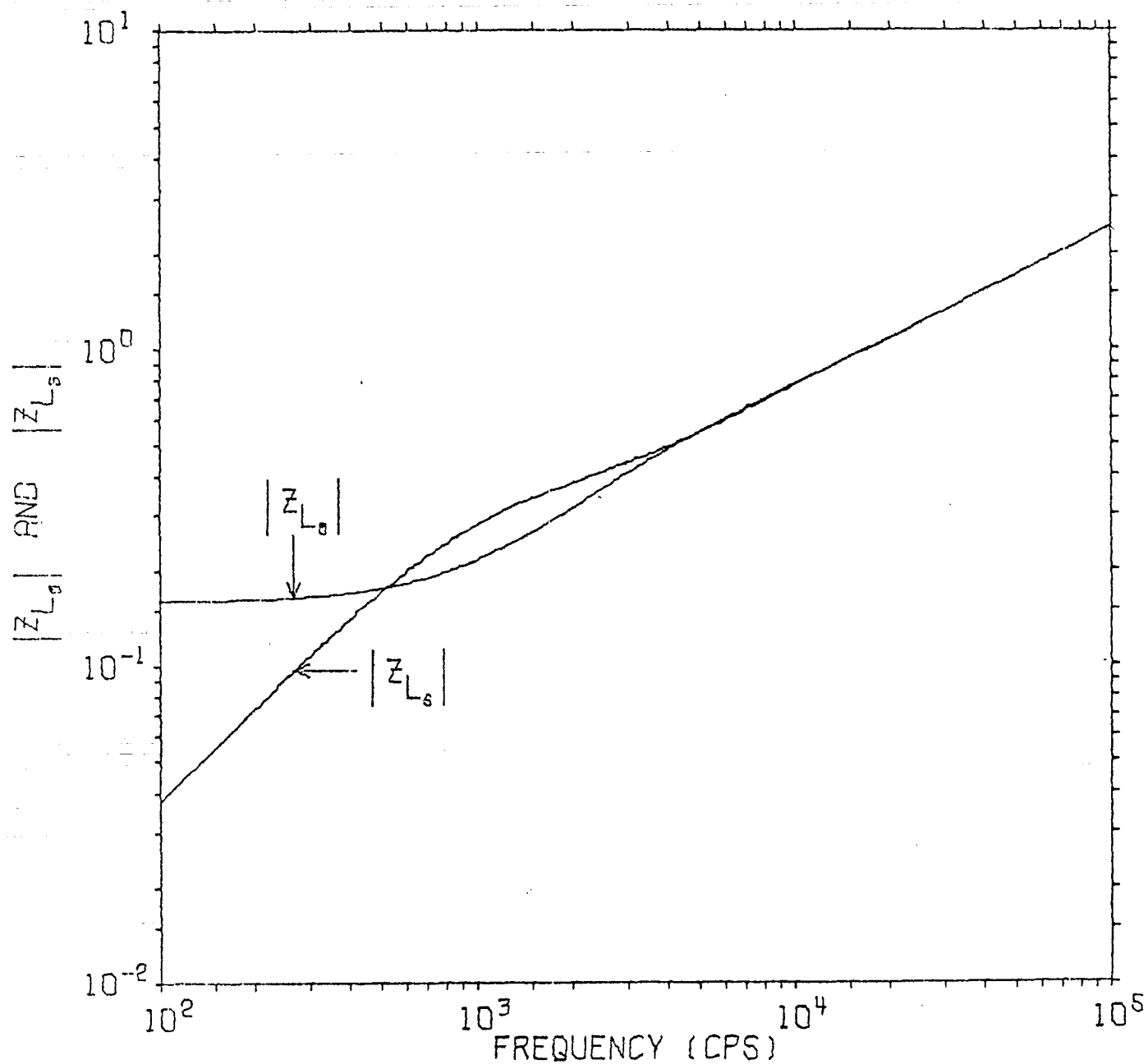
MAGNITUDE OF OPEN-CIRCUITED AND SHORT-CIRCUITED TRANSMISSION
 LINE IMPEDANCE VERSUS FREQUENCY FOR
 $L = 100.0$ METERS, CONDUCTIVITY $= 8.00E-03$ MHOS/METER
 $FG = .473$ ($B/A = 1.00$)



MAGNITUDE OF OPEN-CIRCUITED AND SHORT-CIRCUITED TRANSMISSION
 LINE IMPEDANCE VERSUS-FREQUENCY FOR
 L = 100.0 METERS, CONDUCTIVITY = 1.10E-02 MHOS/METER
 FG = .473 (B/A = 1.00)



MAGNITUDE OF OPEN-CIRCUITED AND SHORT-CIRCUITED TRANSMISSION
 LINE IMPEDANCE VERSUS FREQUENCY FOR
 $L = 100.0$ METERS, CONDUCTIVITY = $3.00E-02$ MHOS/METER
 $FG = .473$ ($B/A = 1.00$)



Program EXAMN

Program EXAMN accepts parameters from data cards as follows:

<u>Variable Name</u>	<u>Column</u>	<u>Type</u>	<u>Format by Which Variable is Read</u>	<u>Use</u>
STOPRD	1	Alpha-numeric	1A1	Stops reading cycle
FG	2-8	Real	F9.8	Geometric factor
BA	10-15	Real	F5.2	Ratio of the distance between the plates to the plate length (for clarification only)
L	20-25	Real	F7.2	Depth of the plate into the ground
SIGMA	30-35	Real	E9.2	Conductivity of ground

The program generates one graph for each data card that it reads except the last data card which should contain an asterisk (*) in the first column to stop the reading cycle. The graphs drawn by EXAMN are logarithmic vertically and horizontally. The plots measure six inches by six inches.

The domain of the frequency consists of three consecutive decades between 10^2 and 10^7 . The program determines this domain in order to calculate values of $|Z_{L_o}|$ and $|Z_{L_s}|$ in an area of interest. The range, R , of $|Z_{L_o}|$ and $|Z_{L_s}|$ is $10^{-1} \leq R \leq 10^2$ unless $Z_{L_s} = f(F(1))$ is less than 10^{-1} in which case the range is shifted so that $10^{-2} \leq R \leq 10^1$.

The program generates approximately 50 values of the frequency for each of the three decades and calculates corresponding values for $|Z_{L_o}|$ and

$|Z_{L_s}|$. The numbers are listed by the printer along with the parameters that determine them.

Subroutine ADJUST is called in the event values of $|Z_{L_o}|$ and $|Z_{L_s}|$ fall beyond the upper limit of the range for the selected domain. This routine adjusts the data to the extent of retaining only those points within the upper limits of the graph. The adjusted points are then plotted.

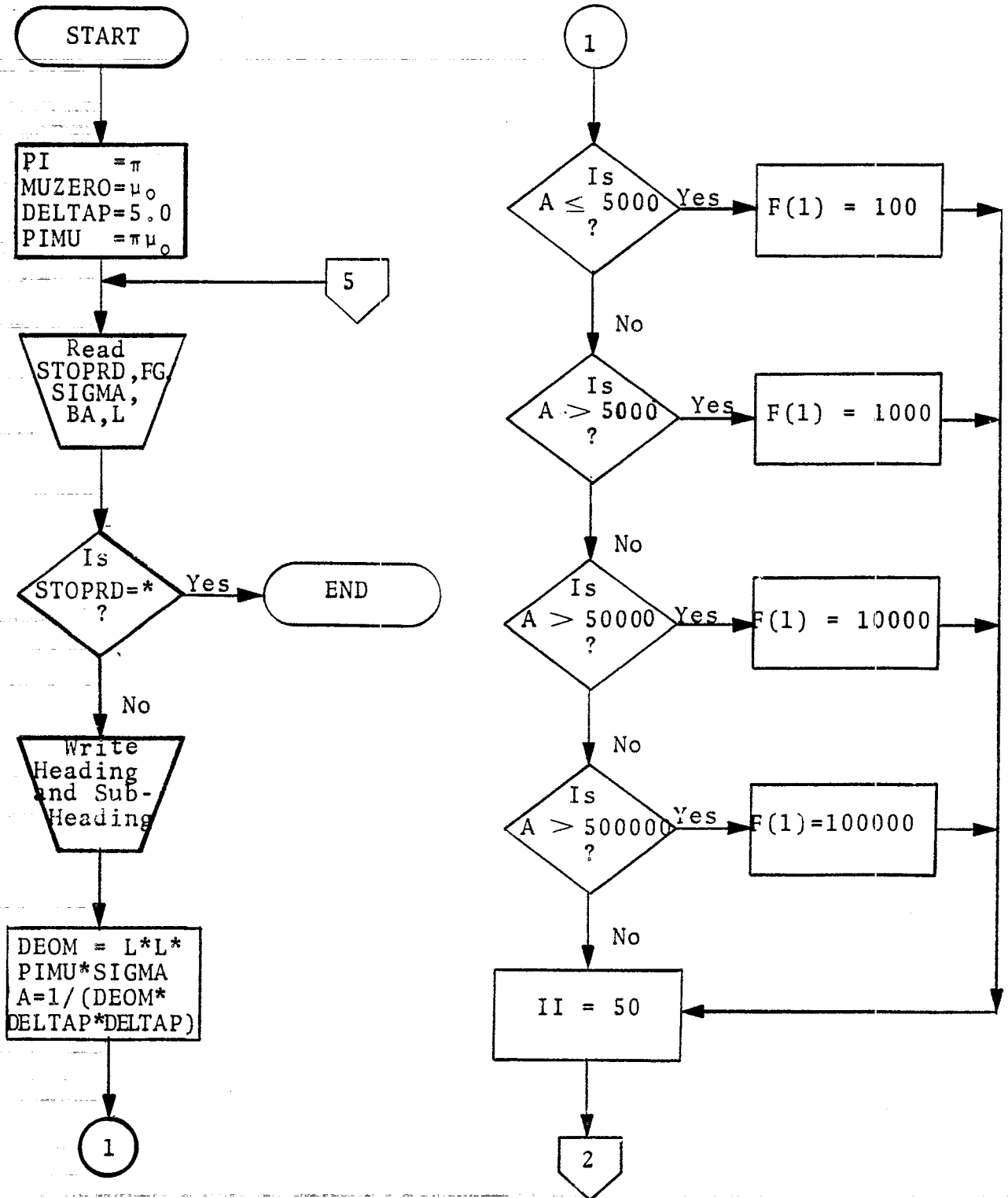
Output to the Calcomp Plotter consists of, for each data card, a log-log graph of f versus $|Z_{L_o}|$ and f versus $|Z_{L_s}|$ along with a heading listing the three parameters. Differentiating tags are positioned at the tenth point plotted for each curve.

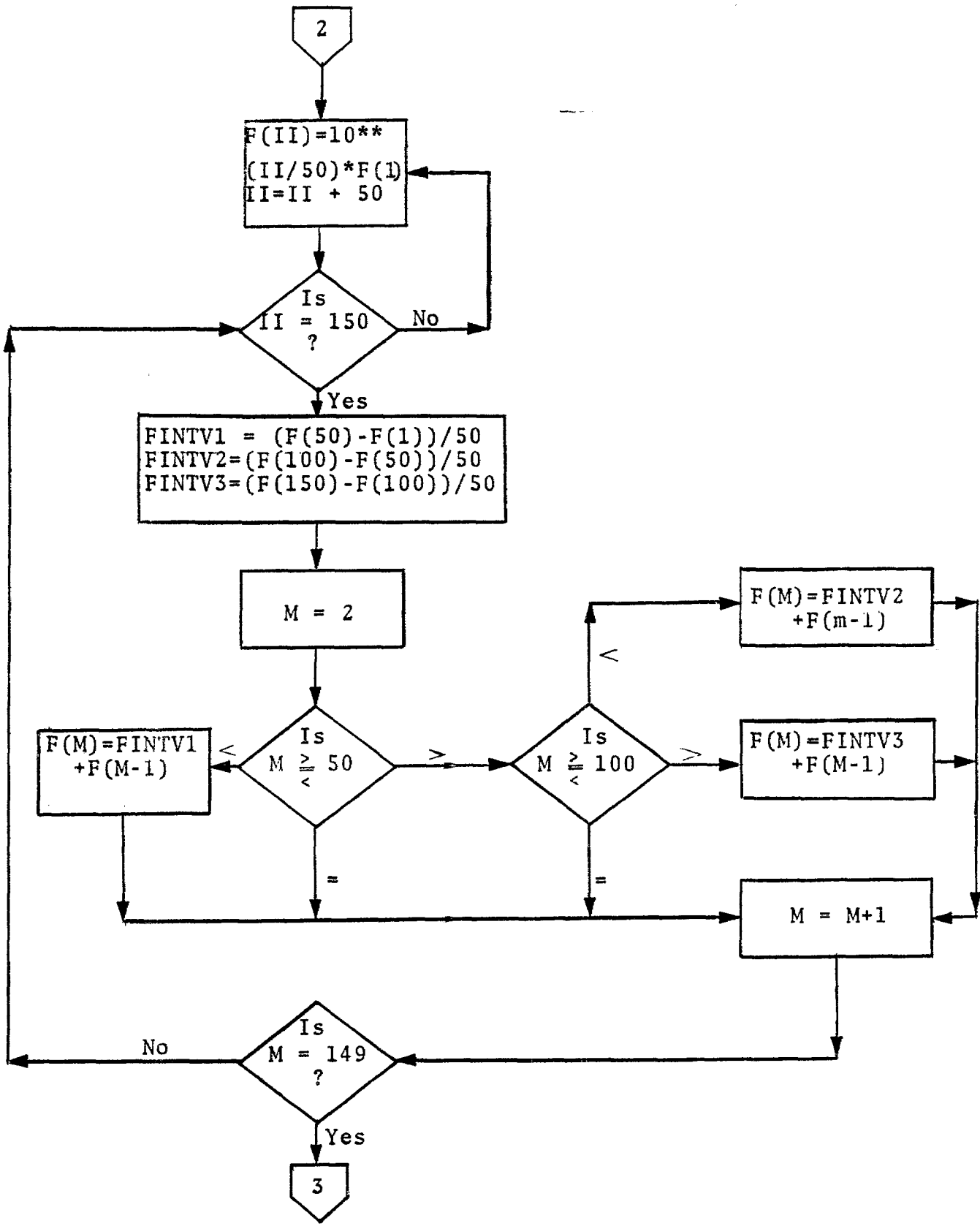
One one-half inch plot tape is required by Program EXAMN. The Calcomp Plotter instructions are written on this tape and it must be specified as a low density tape (200 BPI). The logical designation for this tape is 10 and must appear as such in the control cards.

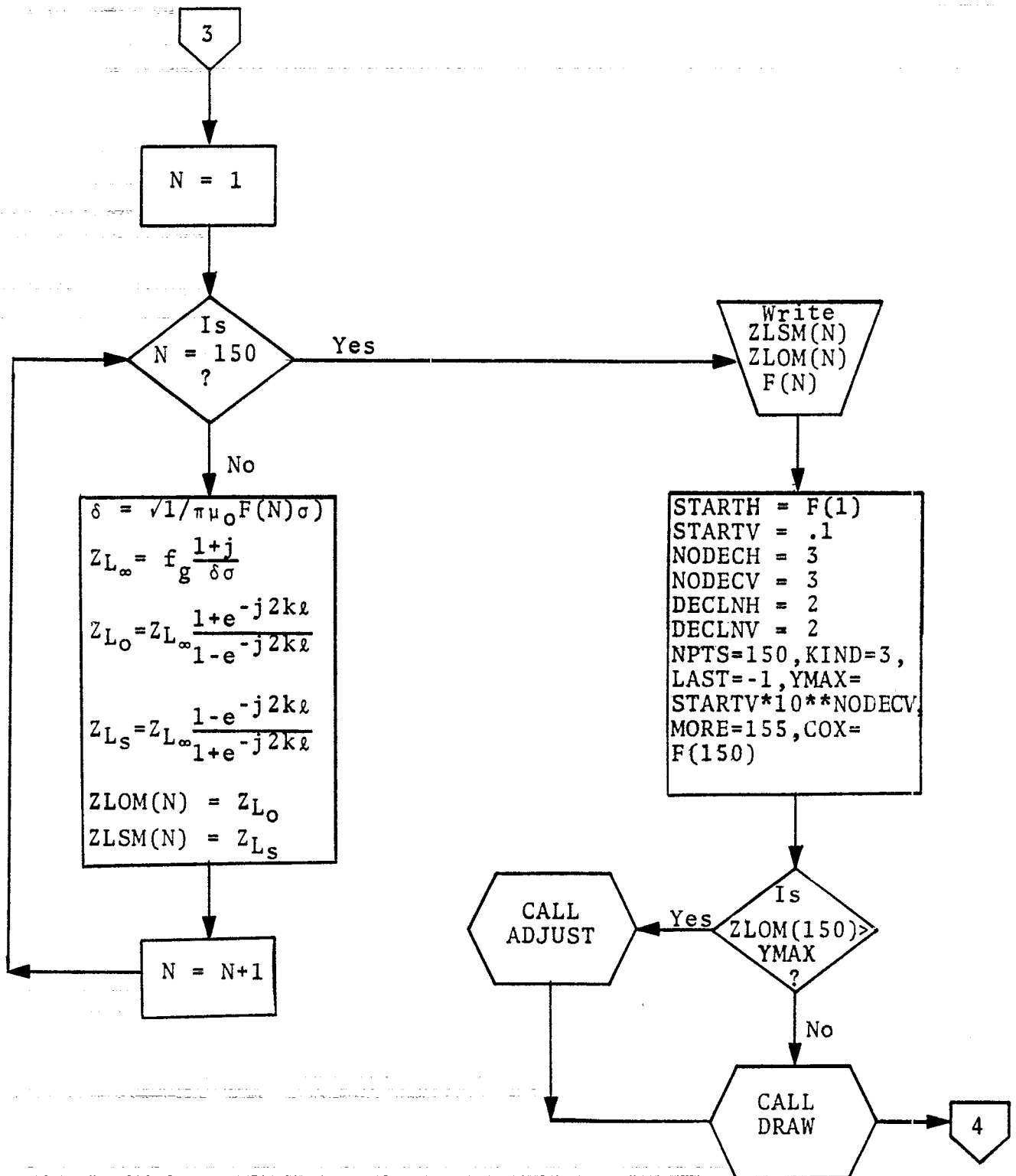
CPU time to compile and produce the first graph is approximately 27 seconds. Each subsequent graph takes less than five seconds. The program will compile and execute in a field of $(53000)_8$. These figures are based on the use of the CDC Chippewa Fortran System on a CDC 6600 computer.

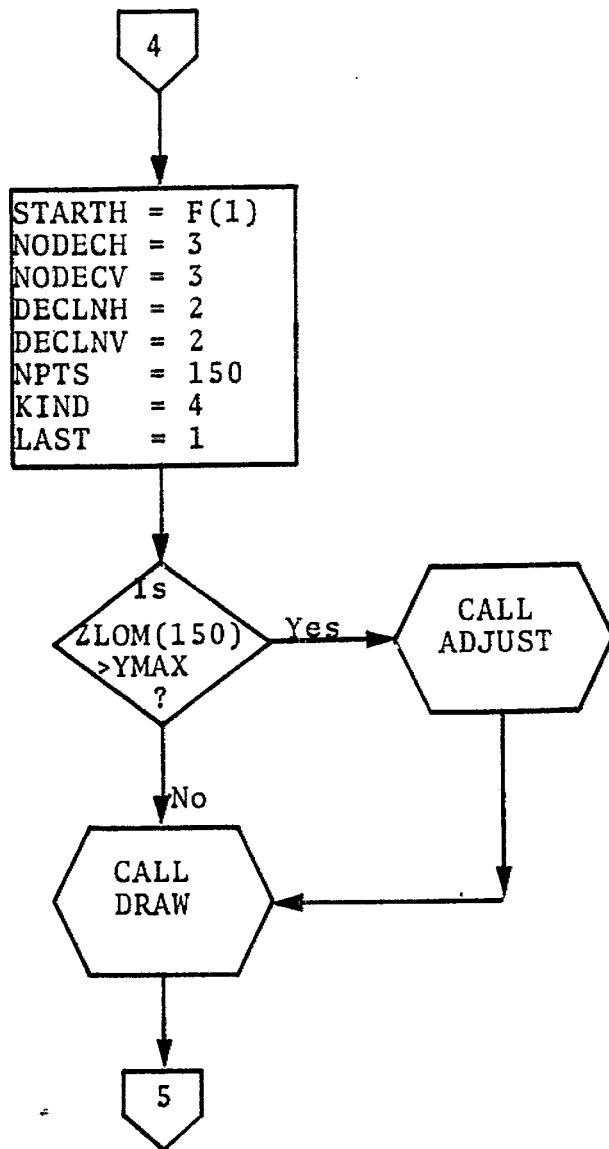
Appendix A

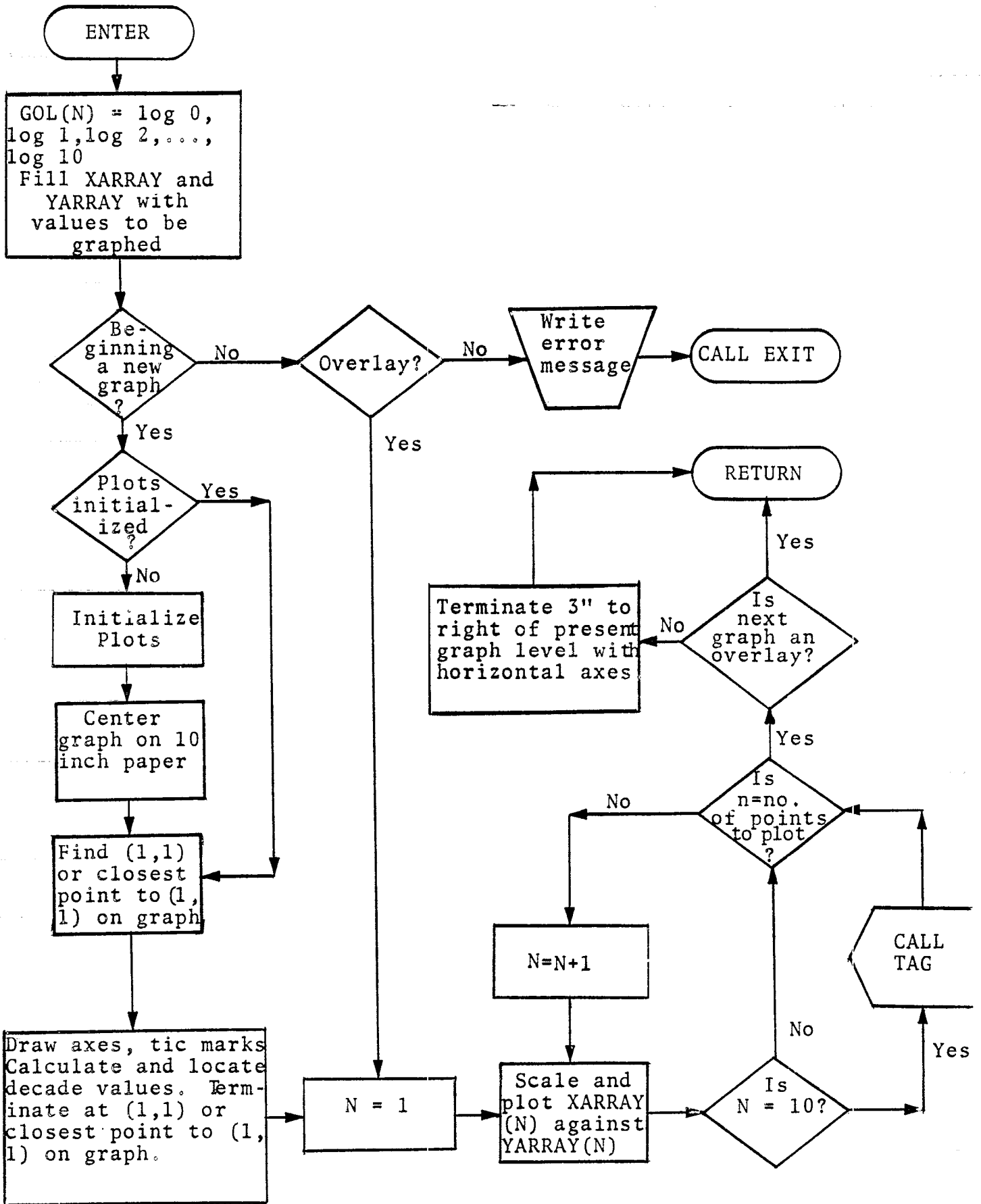
Flow Charts for Program EXAMN











Appendix B

Program Listing

```

C      PROGRAM  EXAMN(INPUT,OUTPUT,TAPF5=INPUT,TAPF6=OUTPUT,TAPF10)      EX  1
C*****
C
C          A T H R E E  P A R A M E T E R  S T U D Y  O F
C
C          S E N S O R  A N D  S I M U L A T I O N  N O T E  2  2
C
C          T H E  O P E N - C I R C U I T E D  A N D  S H O R T - C I R C U I T E D  T R A N S M I S S I O N  L I N E
C          S I M U L A T I O N  F O R  B U R I E D  S T R U C T U R E S  I S  E X A M I N E D .
C
C          T H I S  P R O G R A M  R E A D S  T H E  G E O M E T R I C  F A C T O R ,
C          D E P T H  O F  T R A N S M I S S I O N  L I N E ,  A N D  G R O U N D  C O N D U C T I V I T Y ,
C          A N D  R E T U R N S  G R A P H S  O F  F R E Q U E N C Y  V E R S U S
C          M A G N I T U D E  O F  T H E  I M P E D A N C E .
C
C*****
C      COMPLEX ETOX,C1,C2,ZIDEAL,ZLO,ZO,ZLS      EX  2
C      REAL MUZERO,L      FX  3
C      DIMENSION F(200),ZLOM(200),ZLSM(200),XF(200),YF(200)      FX  4
C      DATA STAR/1H*/      FX  5
C      PI=3.14159265358979      FX  6
C      MUZERO=.00000125663706143591      FX  7
C      PIMU=PI*MUZERO      FX  8
C      DELTAP=1.0      EX  9
C      C1=CMPLX(1.0,1.0)      FX 10
5      READ (5,10) STOPRD,FG,BA,L,SIGMA      FX 11
10     FORMAT (1A1,F9.8,2X,F5.2,2X,F7.2,2X,E9.2)      FX 12
       IF (STOPRD.EQ.STAR) GO TO 105      EX 13
       WRITE (6,15) L,SIGMA,FG,BA      FX 14
15     FORMAT (1H1,30X,60HMAGNITUDE OF OPEN-CIRCUITED AND SHORT-CIRCUITED EX 15
1 TRANSMISSION/42X,35HLINE IMPEDANCE VERSUS FREQUENCY FOR/30X,13HPL FX 16
2 ATE DEPTH =,F5.1,23H METERS, CONDUCTIVITY =,E9.2,11H MHOS/METER/40 FX 17
3 X,23HGEOMETRIC FACTOR (FG) =,F6.4,7H (B/A =,F5.2,1H)      EX 18
       WRITE (6,20)      EX 19
20     FORMAT (1H0,2X,9HFREQUENCY,4X,4HZLOM,6X,4HZLSM,16X,9HFREQUENCY,4X, EX 20
14HZLOM,6X,4HZLSM,16X,9HFREQUENCY,4X,4HZLOM,6X,4HZLSM)      EX 21
       DEOM=L*L*PIMU*SIGMA      EX 22
       A=1.0/(DEOM*DELTAP*DELTAP)      EX 23
       IF(A.LE.5000.)F(1)=100.      EX 24
       IF(A.GT.5000.)F(1)=1000.      FX 25
       IF(A.GT.50000.)F(1)=10000.      FX 26
       IF(A.GT.500000.)F(1)=100000.      EX 27
35     DO 40 II=50,150,50      EX 28
40     F(II)=10**(II/50)*F(1)      EX 29
       FINTV1=(F(50)-F(1))/50.      EX 30
       FINTV2=(F(100)-F(50))/50.      FX 31
       FINTV3=(F(150)-F(100))/50.      EX 32
       DO 65 M=2,149      EX 33
       IF (M-50) 45,65,50      EX 34

```

45	F(M)=FINTV1+F(M-1)	FX	35
	GO TO 65	FX	36
50	IF (M-100) 55,65,60	FX	37
55	F(M)=FINTV2+F(M-1)	FX	38
	GO TO 65	EX	39
60	F(M)=FINTV3+F(M-1)	EX	40
65	CONTINUE	EX	41
	DO 70 N=1,150	EX	42
	DELTA=SQRT(1.0/(PI*F(N)*SIGMA))	EX	43
	ZIDEAL=FG*C1/(DELTA*SIGMA)	EX	44
	B=L*(-2.0/DELTA)	EX	45
	C2=CMPLY(B,B)	EX	46
	ETOX=CEXP(C2)	EX	47
	ZLO=ZIDEAL*(1.0+ETOX)/(1.0-ETOX)	EX	48
	ZLOM(N)=CABS(ZLO)	EX	49
	ZLS=ZIDEAL*(1.0-ETOX)/(1.0+ETOX)	EX	50
	ZLSM(N)=CABS(ZLS)	EX	51
70	CONTINUE	EX	52
	WRITE (6,75) ((F(NN),ZLOM(NN),ZLSM(NN),F(NN+50),ZLOM(NN+50),ZLSM(NN+50)),NN=1,50)	EX	53
	FORMAT (1X,3E10.2,13X,3F10.2,13X,3E10.2)	EX	54
75	STARTR=F(1)	EX	55
	IF(ZLSM(1).LT..1) STARTV=.01	EX	56
	IF(ZLSM(1).GE..1) STARTV=.1	EX	57
	NODECH=3	EX	58
	NODECV=3	EX	59
	DECLNH=2.	EX	60
	DECLNV=2.	EX	61
	NPTS=150	EX	62
	KIND=3	EX	63
	LAST=-1	EX	64
	YMAX=STARTV*10.**NODCV	EX	65
	MORE=155	EX	66
	COX=F(150)	EX	67
	IF(ZLOM(150).GT.YMAX) GO TO 80	EX	68
	GO TO 85	EX	69
80	CALL ADJUST(F,ZLOM,NPTS,COX,YMAX,XF,YF,MORE,NEWPTO)	EX	70
	CALL DRAWL(STARTR,STARTV,NODECH,NODECV,DECLNH,DECLNV,NEWPTO,XF,	EX	71
	LYF,KIND,LAST,BACK)	EX	72
	GO TO 90	EX	73
95	CALL DRAWL(STARTR,STARTV,NODECH,NODECV,DECLNH,DECLNV,NPTS,F,ZLOM,	EX	74
	IKIND,LAST,BACK)	EX	75
90	STARTR=F(1)	EX	76
	NODECH=3	EX	77
	NODECV=3	EX	78
	DECLNH=2.	EX	79
	DECLNV=2.	EX	80
	NPTS=150	EX	81
	KIND=4	EX	82
		EX	83

	LAST=1	EX 84
	IF(7LDM(150).GT.YMAX) GO TO 95	EX 85
	CALL DRAWL (STARTR,STARTV,NODECH,NODECV,DECLNH,DECLNV,NPTS,F,ZLSM,	EX 86
	IKIND,LAST,BACK)	EX 87
	GO TO 100	EX 88
95	CALL ADJUST(F,ZLSM,NPTS,COX,YMAX,XF,YF,MORE,NEWPTS)	EX 89
	CALL DRAWL (STARTR,STARTV,NODECH,NODECV,DECLNH,DECLNV,NEWPTS,XF,	EX 90
	1YF,KIND,LAST,BACK)	EX 91
100	CALL HEAD(6.,6.,L,SIGMA,FG,BA,BACK)	EX 92
	GO TO 5	EX 93
105	CONTINUE	EX 94
	END	EX 95

```

SUBROUTINE DRAWL (STARTH,STARTV,NODECH,NODECV,DECLNH,DECLNV,NPTS,X TL 1
IARRAY,YARRAY,KIND,IAST,XT) TL 2
C*****
C THIS SUBROUTINE SCALES, DRAWS THE AXIS FOR THE LOG LOG GRAPH, AND *
C PLOTS THE DATA WITH ANY NUMBER OF OVERLAYS ON THE CALCOMP PLOTTER. *
C*****
DIMENSION X(200), Y(200), GOL(11), XARRAY(NPTS), YARRAY(NPTS) TL 3
DATA GOL/0.0,.17609,.30103,.47712,.60206,.69897,.77815,.84510,.903 TL 4
109,.95424,1.0/,IFT/2HI2/,CORECY/0./,CORECX/0./,JFT/2HI1/ TL 5
DO 5 I=1,NPTS TL 6
X(I)=XARRAY(I) TL 7
5 Y(I)=YARRAY(I) TL 8
THROKK=KIND TL 9
IF (KIND-3) 15,25,10 TL 10
IF (KIND-4) 15,150,15 TL 11
15 WRITE (6,20) KIND TL 12
20 FORMAT (41H THE KIND OF GRAPH ASKED FOR IS IN ERROR,I8) TL 13
RETURN TL 14
25 IF (I0-2) 30,35,30 TL 15
30 CALL PLOTS (TB,TB,I0) TL 16
I0=2 TL 17
RNODEC=NODECV TL 18
REALH=RNODEC*DECLNV TL 19
YS=(10.-REALH)/2.-.5 TL 20
CALL PLOT (0.,YS,-3) TL 21
35 K=0 TL 22
CALL FLAG (K,STARTH,NODECH) TL 23
K=3*(K-1) TL 24
CALL FLAG (K,STARTV,NODECV) TL 25
GO TO (40,45,50,55,60,65,70,75,80), K TL 26
40 CALL FIND1 (STARTH,NODECH,DECLNH,XXX) TL 27
CALL FIND1 (STARTV,NODECV,DECLNV,YYY) TL 28
GO TO 85 TL 29
45 CALL TOSMAL (STARTV,NODECV,CORECY,YYY,DECLNV) TL 30
CALL FIND1 (STARTH,NODECH,DECLNH,XXX) TL 31
GO TO 85 TL 32
50 CALL TOLARG (STARTV,NODECV,CORECY,YYY) TL 33
CALL FIND1 (STARTH,NODECH,DECLNH,XXX) TL 34
GO TO 85 TL 35
55 CALL TOSMAL (STARTH,NODECH,CORECX,XXX,DECLNH) TL 36
CALL FIND1 (STARTV,NODECV,DECLNV,YYY) TL 37
GO TO 85 TL 38
60 CALL TOSMAL (STARTH,NODECH,CORECX,XXX,DECLNH) TL 39
CALL TOSMAL (STARTV,NODECV,CORECY,YYY,DECLNV) TL 40
GO TO 85 TL 41
65 CALL TOSMAL (STARTH,NODECH,CORECX,XXX,DECLNH) TL 42
CALL TOLARG (STARTV,NODECV,CORECY,YYY) TL 43

```

	GO TO 85	TL 44
70	CALL TOLARG (STARTR,NODECH,CORECX,XXX)	TL 45
	CALL FIND1 (STARTV,NODECV,DECLNV,YYY)	TL 46
	GO TO 85	TL 47
75	CALL TOLARG (STARTR,NODECH,CORECX,XXX)	TL 48
	CALL TOSMAL (STARTV,NODECV,CORECY,YYY,DECLNV)	TL 49
	GO TO 85	TL 50
80	CALL TOLARG (STARTR,NODECH,CORECX,XXX)	TL 51
	CALL TOLARG (STARTV,NODECV,CORECY,YYY)	TL 52
85	NODECH=NODECH+1	TL 53
	NODECV=NODECV+1	TL 54
	XX=0.	TL 55
	POWERX=ALOG10(STARTR)	TL 56
	ILOG=POWERX+SIGN(.000001,POWERX)	TL 57
	DO 100 I=1,NODECH	TL 58
	REALI=I-1	TL 59
	INUM=ILOG+(I-1)	TL 60
	RR=XX-.12	TL 61
	RER=XX+.13	TL 62
	CALL SYMBOL (RR,-.3,.14,2H10,0.,2)	TL 63
	IF (INUM.GE.0.AND.INUM.LT.10) CALL NUMBER (RER,-.21,.10,INUM,0.,JF	TL 64
	1T)	TL 65
	IF (INUM.LT.0.OR.INUM.GE.10) CALL NUMBER (RER,-.21,.10,INUM,0.,IFT	TL 66
	1)	TL 67
	CALL PLOT (XX,0.,3)	TL 68
	IF (I-NODECH) 90,105,90	TL 69
90	DO 95 J=1,11	TL 70
	XX=(GOL(J)+REALI)*DECLNH	TL 71
	CALL PLOT (XX,0.0,2)	TL 72
	CALL PLOT (XX,-.05,2)	TL 73
95	CALL PLOT (XX,0.0,2)	TL 74
100	CONTINUE	TL 75
105	CONTINUE	TL 76
	NODEC=NODECV-1	TL 77
	DO 115 I=1,NODEC	TL 78
	REALI=I-1	TL 79
	DO 110 J=1,11	TL 80
	YY=(GOL(J)+REALI)*DECLNV	TL 81
	CALL PLOT (XX,YY,2)	TL 82
	W=XX+.05	TL 83
	CALL PLOT (W,YY,2)	TL 84
110	CALL PLOT (XX,YY,2)	TL 85
115	CONTINUE	TL 86
	NODEC=NODECH-1	TL 87
	DO 125 I=1,NODEC	TL 88
	RELDEC=NODECH-I	TL 89
	DO 120 J=1,11	TL 90
	XX=DECLNH*(RELDEC-(1.0-GOL(--J+12)))	TL 91
	CALL PLOT (XX,YY,2)	TL 92

	Z=YY+.05	TL 93
	CALL PLOT (XX,Z,2)	TL 94
120	CALL PLOT (XX,YY,2)	TL 95
125	CONTINUE	TL 96
	POWERY=ALOG10(STARTV*10.**((NODECV-1)))	TL 97
	JLOG=POWERY+SIGN(.000001,POWERY)	TL 98
	DO 140 I=1,NODECV	TL 99
	YADD=YY-.07	TL 100
	CALL SYMBOL (-.5,YADD,.14,2H10,0.,?)	TL 101
	RYF=YY+.03	TL 102
	JNUM=JLOG-(I-1)	TL 103
	IF (JNUM.GE.0.AND.JNUM.LT.10) CALL NUMBER (-.25,RYF,.10,JNUM,0.,JF	TL 104
	IT)	TL 105
	IF (JNUM.LT.0.OR.JNUM.GE.10) CALL NUMBER (-.25,RYE,.10,JNUM,0.,JF	TL 106
	1)	TL 107
	CALL PLOT (XX,YY,3)	TL 108
	IF (I-NODECV) 130,145,130	TL 109
130	DO 135 J=1,11	TL 110
	YY=DECLNV*((NODECV-I)-(1.-GOL(-J+12)))	TL 111
	CALL PLOT (XX,YY,2)	TL 112
	W=XX-.05	TL 113
	CALL PLOT (W,YY,2)	TL 114
135	CALL PLOT (XX,YY,2)	TL 115
140	CONTINUE	TL 116
145	CONTINUE	TL 117
	CALL PLOT (XXX,YYY,-3)	TL 118
150	DO 225 I=1,NPTS	TL 119
	IF (X(I).GE.1.) GO TO 165	TL 120
	M=0	TL 121
155	X(I)=X(I)*10.	TL 122
	M=M+1	TL 123
	IF (X(I)-1.) 155,160,160	TL 124
160	REALM=M	TL 125
	XX=(ALOG10(X(I))-REALM+CORECX)*DECLNH	TL 126
	GO TO 180	TL 127
165	N=0	TL 128
170	IF (X(I).LE.10.) GO TO 175	TL 129
	X(I)=X(I)/10.	TL 130
	N=N+1	TL 131
	GO TO 170	TL 132
175	REALN=N	TL 133
	XX=(ALOG10(X(I))+REALN+CORECX)*DECLNH	TL 134
180	IF (Y(I).GE.1.) GO TO 195	TL 135
	M=0	TL 136
185	Y(I)=Y(I)*10.	TL 137
	M=M+1	TL 138
	IF (Y(I)-1.) 185,190,190	TL 139
190	REALM=M	TL 140
	YY=(ALOG10(Y(I))-REALM+CORECY)*DECLNV	TL 141

	GO TO 210	TL 142
195	N=0	TL 143
200	IF(Y(I).LE.10.) GO TO 205	TL 144
	Y(I)=Y(I)/10.	TL 145
	N=N+1	TL 146
	GO TO 200	TL 147
205	REALN=N	TL 148
	YY=(ALOG10(Y(I))+REALN+CORECY)*DECLNV	TL 149
210	IF(I-1) 220,215,220	TL 150
215	CALL PLOT(XX,YY,3)	TL 151
	CALL PLOT(XX,YY,2)	TL 152
	GO TO 225	TL 153
220	CALL PLOT(XX,YY,2)	TL 154
	IF(I.FO.10.AND.IHBOKK.EQ.3)CALL TAG(XX,YY,1)	TL 155
	IF(I.EQ.10.AND.IHBOKK.EQ.4)CALL TAG(XX,YY,-1)	TL 156
225	CONTINUE	TL 157
	IF(LAST) 235,230,230	TL 158
230	RNODEC=NODECH	TL 159
	XT=-XXX+RNODEC*DECLNH+3.	TL 160
	CALL PLOT(XT,-YYY,-3)	TL 161
235	RFTURN	TL 162
	END	TL 163-

```

SUBROUTINE FIND1 (START,NODEC,DECLN,XY)
C*****
C THIS SUBROUTINE LOCATES 1 ON THE VERTICAL OR HORIZONTAL AXIS.
C*****
      STARR=START
      DO 15 I=1,NODEC
      N=I
      IF (ABS(STARR-1.0)-1.0E-6) 20,20,5
5      IF (STARR-1.00) 10,20,20
10     STARR=STARR*10.
15     CONTINUE
20     REALN=N-1
      XY=REALN*DECLN
      RETURN
      END
      F1 1
      *
      *
      F1 2
      F1 3
      F1 4
      F1 5
      F1 6
      F1 7
      F1 8
      F1 9
      F1 10
      F1 11
      F1 12-

```

```

SUBROUTINE TOSMAL (START,NODEC,CORECS,XY,DECLN)
C*****
C
C   TOSMAL DETERMINES THE NUMBER OF DECADES DIFFERENCE BETWEEN 1 AND
C   THE LARGEST VALUE LESS THAN 1.
C*****
C   CORECS=0.0
C   XYMAX=START*10.0**NODEC
C   RELNOD=NODEC
C   XY=RELNOD*DECLN
5   IF (ABS(XYMIN-1.0)-1.0E-6) 20,20,10
10  IF (XYMAX-1.00) 15,20,20
15  CORECS=CORECS+1.
C   XYMAX=XYMAX*10.
C   GO TO 5
20  RETURN
C   END

```

		TS	1
			*
			*
			*
			*
		TS	2
		TS	3
		TS	4
		TS	5
		TS	6
		TS	7
		TS	8
		TS	9
		TS	10
		TS	11
		TS	12-

```

SUBROUTINE TOLARG (START,NODEC,CORECL,XY)
C*****
C
C   TOLARG DETERMINES THE NUMBER OF DECADES DIFFERENCE BETWEEN 1 AND
C   THE SMALLEST VALUE GREATER THAN 1.
C*****
      XY=0.
      CORECL=0.0
      XYMIN=START
5     IF (ABS(XYMIN-1.0)-1.0E-6) 20,20,10
10    IF (XYMIN-1.0) 20,20,15
15    CORECL=CORECL-1.0
      XYMIN=XYMIN*.1
      GO TO 5
20    RETURN
      END

```

TI	1
TL	2
TL	3
TL	4
TL	5
TL	6
TI	7
TL	8
TL	9
TI	10
TI	11-


```

SUBROUTINE HEAD (GL,GH,L,SIGMA,FG,BA,BACK)
C*****
C
C          THIS SUBROUTINE PRINTS THE HEADING AND
C          CORRESPONDING NUMBERS ON THE GRAPH.
C*****
CALL PLOT (-BACK,0.,-3)
GL02=GL/2.
X1=GL02-3.6
X2=GL02-2.16
X3=GL02-3.06
X4=GL02-1.28
X5=GL02-.9
Y1=GH+1.06
Y2=GH+.78
Y3=GH+.5
Y4=GH+.22
Y5=-.5
CALL SYMBOL (X1,Y1,.14,60HMAGNITUDE OF OPEN-CIRCUITED AND SHORT-CI
IRCUITED TRANSMISSION,0.,60)
CALL SYMBOL (X2,Y2,.14,35HLINE IMPEDANCE VERSUS FREQUENCY FOR,0.,3
15)
CALL SYMBOL (X3,Y3,.14,51HL = METERS, CONDUCTIVITY =
1 MHOS/METER,0.,51)
CALL SYMBOL (X4,Y4,.14,22HFG = (B/A = ),0.,22)
CALL SYMBOL (X5,Y5,.14,15HFREQUENCY (CPS),0.,15)
XN1=X3+.36
XN2=X3+3.7
XN3=X4+.38
XN4=X4+2.04
CALL NUMBER (XN1,Y3,.14,L,0.,4HF5.1)
CALL NUMBER (XN2,Y3,.14,SIGMA,0.,4HF9.2)
CALL NUMBER (XN3,Y4,.14,FG,0.,4HF5.3)
CALL NUMBER (XN4,Y4,.14,BA,0.,4HF4.2)
Y6=(GH-1.75)/2.+1
CALL SYMBOL (-.80,Y6,.14,12HZ AND Z,90.,12)
XS1=-.7
YS1=Y6+.12
DO 5 I=1,2
CALL SYMBOL (XS1,YS1,.14,1HL,90.,1)
YS1=YS1+1.32
XS2=-.80+.15
YS2=Y6+.23
CALL SYMBOL (XS2,YS2,.07,1HD,90.,1)
YS2=YS2+1.32
CALL SYMBOL (XS2,YS2,.07,1HS,90.,1)
DO 15 I=1,2
ABST6N=Y6-.05

```

```

HD 1
*****
*
*
*
*
*****
HD 2
HD 3
HD 4
HD 5
HD 6
HD 7
HD 8
HD 9
HD 10
HD 11
HD 12
HD 13
HD 14
HD 15
HD 16
HD 17
HD 18
HD 19
HD 20
HD 21
HD 22
HD 23
HD 24
HD 25
HD 26
HD 27
HD 28
HD 29
HD 30
HD 31
HD 32
HD 33
HD 34
HD 35
HD 36
HD 37
HD 38
HD 39
HD 40
HD 41
HD 42
HD 43

```

```
DO 10 J=1,2
CALL PLOT (-.95,ABSIGN,3)
CALL PLOT (-.65,ABSIGN,2)
10 ABSIGN=ABSIGN+.4
15 Y6=Y6+1.32
CALL PLOT (BACK,0.,-3)
RETURN
END
```

```
HD 44
HD 45
HD 46
HD 47
HD 48
HD 49
HD 50
HD 51-
```

```

SUBROUTINE TAG (X,Y,ISCR1)
C** *****
C SUBROUTINE TAG POINTS OUT AND LABELS THE CURVES ON THE GRAPH.
C *****
C**
ALL PLOT (X,Y,3) TA 2
F (ISCR1) 15,5,20 TA 3
WRITE (6,10) TA 4
10 FORMAT (10X,33HARGUMENT ERROR IN SUBROUTINE TAG.) TA 5
ALL EXIT TA 6
15 X=X+.1 TA 7
Y=Y-.04 TA 8
ALL PLOT (XX,YY,2) TA 9
Y=Y+.04 TA 10
ALL PLOT (XX,YY,3) TA 11
ALL PLOT (X,Y,2) TA 12
X=X+.4 TA 13
ALL PLOT (XX,Y,2) TA 14
Z=XX+.2 TA 15
Y=Y-.07 TA 16
DO TO 25 TA 17
20 X=X+.04 TA 18
Y=Y+.1 TA 19
ALL PLOT (XX,YY,2) TA 20
X=X-.04 TA 21
ALL PLOT (XX,YY,3) TA 22
ALL PLOT (X,Y,2) TA 23
Y=Y+.4 TA 24
ALL PLOT (X,YY,2) TA 25
Z=X-.06 TA 26
Z=Y+.55 TA 27
25 ALL SYMBOL (XZ,YZ,.14,1HZ,0.,1) TA 28
L=XZ+.12 TA 29
L=YZ-.1 TA 30
ALL SYMBOL (XL,YL,.14,1HL,0.,1) TA 31
OS=XZ+.23 TA 32
OS=YZ-.15 TA 33
F (ISCR1) 30,5,35 TA 34
30 ALL SYMBOL (XOS,YOS,.07,1HS,0.,1) TA 35
DO TO 40 TA 36
35 ALL SYMBOL (XOS,YOS,.07,1HO,0.,1) TA 37
40 X=XZ-.1 TA 38
Y=YZ-.15 TA 39
ALL PLOT (XX,YY,3) TA 40
Y=YY+.35 TA 41
ALL PLOT (XX,YY,2) TA 42
X=XZ+.35 TA 43
ALL PLOT (XX,YY,3) TA 44

```

```
YY=YY-.35
CALL PLOT (XX,YY,2)
CALL PLOT (X,Y,3)
RETURN
END
```

```
TA 45
TA 46
TA 47
TA 48
TA 49-
```

```

SUBROUTINE ADJUST(X,Y,NPTS,XM,YM,XF,YF,MORE,L)
C *****
C THIS SUBROUTINE ADJUSTS ALL DATA POINTS IN THE FIRST QUADRANT THAT
C OVERFLOW THE GIVEN LIMITS OF THE BOUNDARY TO THE BOUNDARY WITHOUT THE
C LOSS OF THE SLOPE FROM THE INTERIOR POINT TO THE EXTERIOR POINT
C *****
DIMENSION X(NPTS), Y(NPTS), XF(MORE), YF(MORE)
L=0
I=0
4 I=I+1
IF (I-NPTS) 10,35,45
10 K=0
IF (X(I).GT.XM.AND.X(I+1).GT.XM) GO TO 5
IF (Y(I).GT.YM.AND.Y(I+1).GT.YM) GO TO 5
IF (X(I).GT.XM.OR.X(I+1).GT.XM) K=1
IF (Y(I).GT.YM.OR.Y(I+1).GT.YM) K=K+2
IF (K) 15,40,15
15 C=X(I)
D=Y(I)
F=X(I+1)
F=Y(I+1)
CALL EDGE (C,D,E,F,K,KK,XM,YM)
IF (KK) 5,20,20
20 L=L+1
GO TO (25,30,30), KK
25 XF(L)=C
YF(L)=D
GO TO 5
30 XF(L)=C
YF(L)=D
L=L+1
XF(L)=F
YF(L)=F
GO TO 5
35 IF (X(I).LE.XM.AND.Y(I).LE.YM) GO TO 40
GO TO 45
40 L=L+1
XF(L)=X(I)
YF(L)=Y(I)
GO TO 5
45 RETURN
END
AD 1
AD 2
AD 3
AD 4
AD 5
AD 6
AD 7
AD 8
AD 9
AD 10
AD 11
AD 12
AD 13
AD 14
AD 15
AD 16
AD 17
AD 18
AD 19
AD 20
AD 21
AD 22
AD 23
AD 24
AD 25
AD 26
AD 27
AD 28
AD 29
AD 30
AD 31
AD 32
AD 33
AD 34
AD 35
AD 36
AD 37-

```


95 GO TO 10
JF (Y2-Y1) 105,100,100
100 Y2=YM
KK=2
RETURN
105 Y1=YM
KK=1
RETURN
END

ED 44
ED 45
ED 46
ED 47
ED 48
ED 49
ED 50
ED 51
ED 52